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STS-7 Conceptual Flight Profile

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Mission Planning and Analysis Division

June 1979



Lyndon B. Johnson Space Center

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SHUTTLE PROGRAM

STS-7 CONCEPTUAL FLIGHT PROFILE

IUS/TDRS-A

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June 1979

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1.0 INTRODUCTION AND SUMMARY

The Space Transportation System (STS) Flight Assignment Manifest (ref. 1) has scheduled a Tracking and Data Relay Satellite System (TDRSS) spacecraft (TDRS-A) for a February 1981 launch on STS Flight 7.

This flight design document has been developed by the Mission Planning and Analysis Division (MPAD) in support of the TDRS-A Cargo Integration Review scheduled

This document (Flight 7 Conceptual Flight Profile) contains the preliminary flight profile that conceptually implements the flight requirements and constraints levied by the STS, inertial upper stage (IUS), and the TDRS spacecraft.

The general content of this document consists of the integrated major flight design guidelines and requirements used in the development of the flight profile together with a flight sequence of events and time line that describe the profile and reflect implementation of the integrated set of requirements. Questions concerning this document should be addressed to Jerome Bell/Flight

2.0 Acronyms

AFSCF Air Force satellite control facility AFO abort from orbit abort once around AOA AOS acquisition of signal auxiliary power units APU ASE airborne support equipment ATCS active thermal control system CFP conceptual flight profile center of gravity c.g. CIR cargo integration review time increment Δt ΔV incremental velocity Department of Defense DOD Edwards Air Force Base EAFB EDT eastern daylight time **EPDC** electrical power distribution and control external tank ET EVA extravehicular activity fuel cell power plant FCP fps feet per second flight test requirements FTR FWD foward GET ground elapsed time GMT Greenwich mean time GPC general purpose computer

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GSTDN ground spaceflight tracking and data network
ha apogee altitude

hp perigee altitude

IMU inertial measurement unit'

IUS ____inertial upper stage

JSC Johnson Space Center

KSC Kennedy Space Center

LH local horizontal

LOPT landing opportunity

LOS loss of signal

LV local vertical

LVLH local vertical/local horizontal

MECC main engine cutoff

MPAD Mission Planning and Analysis Division

MPS main propulsion subsystem

NPC nonpropulsive consumables

OA Orbiter after

OMS orbital maneuvering system

OMS-1 first OMS maneuver

OMS-2 second OMS maneuver

OP Orbiter prior

PET phase elapsed time

PI payload integrator

PIP payload integration plan

PLBD payload bay doors

PROP propellant

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pounds per square foot psf passive thermal control PTC maximum dynamic pressure qmax reaction control system (Primary) RCS radio frequency RF remote manipulator system RMS return-to-launch site RTLS remote tracking stations RTS Shuttle payload integration and development program office SPIDPO solid rocket booster SRB IUS stage-1 solid rocket motor SRM-1 IUS stage-2 solid rocket motor SRM-2 Space Shuttle main engine SSME star tracker ST space transportation system STS Shuttle vehicle SV to be determined TBD thermal control system TCS tracking and data relay satellite TDRS first TDRS spacecraft TDRS-A tracking and data relay satellite system **TDRSS** thrust vector control system TVCS vernier reaction control system VRCS western test range WTR payload-bay-to-Earth attitude -ZLV

3.0 GUIDELINES AND GROUNDRULES

3.1 GENERAL FLIGHT REQUIREMENTS

- a. The launch date is February 27, 1981.
- b. Nominal end-of-mission shall be planned for 2 days.
- c. The nominal post-Orbiter maneuvering system-2 (OMS-2) parking orbit is 150 n. mi. circular.
- d. At the time of deployment, the minimum parking orbit shall be the equivalent of a 150 n. mi. circular orbit.
- e. The nominal parking orbit inclination is 28.48 degrees.
- f. The launch and landing site is Kennedy Space Center (KSC)
- g. The payload complement consists of a tracking and data relay satellite (TDRS-A) spacecraft integrated on a Department of Defense (DOD) 2-stage inertial upper stage (IUS), the IUS airborne support equipment (ASE), and the necessary space transportation system (STS) cargochargeable equipment required to interface the IUS vehicle with the Orbiter.
- h. The crew size is four.
- i. Orbiter vehicle 102 configuration per reference 2 will be used.
- j. The capability shall be provided to allow a return from orbit without having to deploy the IUS/TDRS.
- k. Launch window shall be selected to prevent nominal end-of-mission or abort landings from occurring prior to sunrise or later than sunset.
- 1. Return-to-launch site (RTLS) and abort-once-around (AOA) landings will be planned to be at KSC.
- m. Provide the consumables loading to allow a landing within 7 hours GET for an abort from orbit (AFO).
- n. A backup landing opportunity will be provided one revolution after nominal landing.
- o. The maximum space Shuttle main engine (SSME) thrust for nominal ascent is 100 percent; for aborts, the maximum thrust is 109 percent.
- p. Liftoff, end-of-mission, and abort landing payload weights are per the Payload Data Annex to the TDRS Payload Integration Plan (PIP).

- q. The payload bay doors (FLBD) are to be opened as soon as operationally convenient after OMS-2, however keeping the PLBD closed for up to 3 hours after launch shall not preclude continuation of the mission.
- r. The TDRS command and telemetry links must be checked out onorbit prior to deployment. The nominal path will be: Ground spaceflight tracking and data network (GSTDN), Orbiter, Payload Interrogator, and TDRS.
- s. One opportunity shall be provided for a direct TDRS to GSTDN radio frequency (RF) check prior to deployment. This is a contingency operation.
- t. When the PLBD are open, the Orbiter will fly a payload bay to Earth (-ZLV) attitude except during the following activities:
 - (1) All Orbiter inertial measurement unit (IMU) alinements
 - (2) TDRS/STDN direct RF check
 - (3) IUS attitude initialization
 - (4) IUS/TDRS deployment operation
 - (5) Preentry thermal conditioning, as required
- u. The nominal geosynchronous placement longitude is 53 degrees west.
- v. The maximum payload allowance will be based on two sigma flight performance reserve loading for AOA.
- w. There will be four potable water tanks available for cooling using the flash evaporator. Also, one additional waste water tank can be used for additional cooling during aborts and contingencies. The potable water tanks will be 95 percent full for normal entry.
- x. For nonpropulsive consumables budgeting, the following contingencies will be considered.
 - (1) A 24-hour hold without reservice
 - (2) The worst case of the following:
 - (a) Cabin puncture
 - (b) One extravehicular activity (EVA)
 - (c) Last deorbit opportunity on mission extension day
 - (d) One cabin repressurization
 - (e) Deorbit one orbit late

- y. Computation and communications required to develop and transmit a ground navigation state vector and Orbiter maneuver include the following:
 - (1) Tracking passes over at least three stations distributed during one complete revolution are required to acquire enough data for computing an accurate ground navigation state vector.
 - (2) Two additional tracking passes are required to provide backup and maintain ravigation accuracy in the event of tracking station loss during one of the passes in (1) above. These backup passes may be located either before, after, or before and after the tracking interval in (1) above.
 - (3) All station passes should be above 3 degree ground station elevation.
 - (4) Fifteen minutes are required for ground computation of state vector.
 - (5) Twenty minutes are to be allocated for computation of the Orbiter maneuver and uplink pads given the above state vector as input.
 - (6) One primary and one backup station pass are required for uplinking the state vector and/or maneuver data.
- z. When possible, deorbit should be executed on a path that allows tracking by a station between deorbit cutoff and entry interface. This station pass must be at a minimum of 14 degree elevation.
- aa. Propellant loading for attitude control shall be planned on the hasis of using primary RCS only. The resulting propellant loading will be needed in the event of a failure of the vernier RCS.
- bb. The IUS flight operations requirements and constraints are as presented to the Shuttle Payload Integration and Development Program Office (SPIDPO) at the Johnson Space Center (JSC) 17 April 1979 and documented in a letter from Col. Shaffer, IUS Program Director, to G. Lunney, Manager, SPIDPO.
- cc. The TDRS flight requirements and constraints are as defined in the TDRS PIP, 19 April 1979.
- dd. The detailed TDRS/IUS data required for flight design implementation are as defined in the TDRS/IUS PIP annexes.
- ee. The Orbiter separation sequence will be designed in accordance with the criteria and philosophy contained in formal briefings to STS management (references 3 and 4).
- ff. 900-n. mi. crossrange operational capability for landing will be assumed.

- gg. The solid rocket booster (SRB) configuration is the TC-121-78 and uses the Western Test Range (WTR) burn rate.
- hh. There is no SRB ignition delay.
- ii. SSME propellant line screens are assumed to be removed for this flight.
- jj. The abort decision lag time is zero.

4.0 FLIGHT DESCRIPTION

This section describes the nominal mission profile. An integrated flight activities time line is found in figure 1, and the integrated major events table is shown in table ${\tt I}$.

Orbiter Earth groundtracks for the entire flight are shown in figure 2, and the Orbiter attitude time line is presented in table II. Table III gives the separation maneuver summary of events while figure 3 depicts the composite launch window. The Orbiter weight summary utilizing data from reference 1 are found in table IV. Figure 4 is a diagram depicting the Orbiter, IUS, and TDRS coordinate systems.

The ground spacecraft tracking and data network (GSTDN), for Orbiter and TDRS support and the Department of Defense's AFSCF remote tracking stations (RTS), for IUS support, will be used for this flight. The assumed communications network is found in table V. Figure 5 shows the IUS and TDRS-A (OMNI) pattern. Table VI presents data on the GSTDN and RTS coverage. Figure 6 shows onorbit pictorial summaries and table VII shows Flight 7 communication and navigation opportunities. Figure 7 depicts relative motion between the Orbiter and IUS-TDRS-A postseparation. Table VIII shows sunrise/sunset data. Table IX and figure 8 present the nonpropulsive consumables loading data. Table X gives data on OMS and RCS budgets.

4.1 LAUNCH WINDOW

The STS-7 launch window for a February 27, 1981 launch date opens at 19:34:35 GMT and closes at 20:16:33 GMT. Nominal lift-off time for this flight is planned for the opening of the launch window, 19:35:00 GMT. The 42-minute launch window duration results solely from the TDRS-A requirement to achieve a right ascension of the ascending node of the placement orbit between 275 degrees and 290 degrees. It is compatible with descending node transfer orbit injection opportunities on the first day and ascending node transfer orbit injection opportunities on the second day that achieve longitude placement within a 53° W to 99° W range at geosynchronous orbit arrival. The latest launch can occur and still maintain the daylight landing constraint is 20:50:00 GMT regardless of TDRS-A requirements. An integrated launch window is summarized in figure 3. This figure shows the available launch window for all components that define the composite launch window.

4.2 FLIGHT PROFILE SUMMARY

4.2.1 Ascent to OMS-2

The Shuttle will be launched from KSC on a 90.0-degree launch azimuth on February 27, 1981. Launch time is 19:35:00 GMT (14:35:00 EST, February 27, 1981, KSC local time). Nominal main engine cutoff (MECO) occurs 8 minutes 10.00 seconds after launch, inserting the Orbiter into a 78.0- by -12.0-n. mi. orbit. The Orbiter is in a payload-bay-to-Earth attitude.

The external tank (ET) is jettisoned and 120.0 seconds after MECO an OMS-1 burn is performed raising the apogee of the Orbiter orbit to 150.0 n. mi. and perigee to 56.0 n. mi. This is a 211.0 fps maneuver with a burn time of approximately 131.0 seconds.

An OMS-2 maneuver is performed at apogee of the 150.0- by - 56.0-n. mi. orbit about 35.5 minutes after the OMS-1 burn (45:43.0 GET). This 169.0 fps maneuver, of approximately 105.0 seconds duration, circularizes the orbit at 150.0 n. mi.

4.2.2 OMS-2 to Deployment

The PLED are opened 35 minutes after completion of the OMS-2 maneuver at 1 hour 20 minutes GET. To fulfill payload thermal requirements and constraints, the Orbiter maintains a payload-bay-to-Earth (-ZLV) attitude except during those operations requiring special attitudes; e.g., star scan maneuvers, RF communications, IMU alinements, and deployment operations. These activities are either in darkness passes or in the shadow of the Orbiter.

At 1 hour 55 minutes GET, an IMU alinement is performed to support normal Orbiter procedures. Following the IMU alinement, a block of time from 2 hours 25 minutes to 6 hours 15 minutes GET is devoted to early Orbiter postinsertion operations. The first activities in this time period are an early IUS health check followed by an early TDRS-A payload interrogator (PI) command link check over the MIL tracking station. The Orbiter then performs a star scan maneuver to support the IUS attitude initialization test. These data are downlinked. and a state vector is uplinked along with the postinsertion trim maneuvers. These trim maneuvers, performed to arrest insertion dispersions and trim the Orbiter into the nominal deployment orbit, are executed between 4 hours 57 minutes and 6 hours 15 minutes GET. Although it is planned to execute these as RCS maneuvers in a -ZLV attitude, the precise method of execution will be developed as part of the flight control and crew procedures development activities. The time line and performance budgets presented in this CFP are based on a maximum of two RCS trim maneuvers, budgeted up to 15 fps, executed within one revolution.

Operations that support deployment begin at 6 hours 23 minutes GET and continue through deployment. Initially, the Orbiter performs an IMU alinement to support the final IUS attitude initialization maneuvers which begin at 7 hours 53 minutes GET. At 8 hours 37 minutes GET, the Orbiter is over the IOS track station. During this pass the predeployment checkout is performed along with an uplink of the Orbiter state vector and an update to the deployment time and attitude. The HAW pass will serve as a backup for these activities.

The Orbiter then performs an attitude maneuvering sequence to achieve the deployment attitude. Since these maneuvers occur in daylight, the sequence is done in such a manner that the Orbiter constantly shades the P/L from the Sun and ends with the Orbiter in the inertial deployment attitude. These maneuvers begin at 8 hours 53 minutes GET. After the Orbiter is in the deployment attitude, the tilt table is elevated to 29 degrees. The predeployment TDRS-A checkout, including activation and RF checks through the PI of the TDRS-A transmitter, occurs over the HAW tracking station. This is the last RTS

site available prior to the nominal deployment opportunity. The AGO GSTDN tracking station is a backup for the TDRS-A checkout. If the nominal TDRS-A RF check is unsuccessful a direct ground to TDRS-A RF check is required. The Orbiter would be maneuvered out of the deployment attitude into an inertial attitude that ensures 5 minutes of coverage over AGO. Following the check, the Orbiter would then maneuver back into the deployment attitude.

At 9 hours 58 minutes GET the final deployment operations begin. These operations include switching the IUS to internal power, switching TDRS-A to IUS power, inhibiting all Orbiter maneuvering systems, and raising the tilt table to 58 degrees. The IUS/TDRS-A is then ejected at about .4 fps at 10 hours 5 minutes GET.

The detailed flight time line is presented in table I and figure 1.

4.2.3 Ejection to Deorbit

One minute and 9 seconds after ejection, the Orbiter performs an RCS maneuver sequence to achieve the desired position and attitude for an OMS separation maneuver. At 10 hours 16 minutes GET, 11 minutes after ejection and 1 minute after IUS RCS activation, the OMS separation maneuver is performed. The burn ΔV is 69.0 fps and the duration of the burn is 35 seconds. The resultant Orbiter orbit has a 189-n. mi. apogce and 150-n. mi. perigee. This orbit will place the Orbiter approximately 62 n. mi. behind and 33 n. mi. below the IUS/TDRS-A at SRM-1 ignition. After the OMS separation maneuver, the Orbiter orients to an IUS viewing attitude (PLBD in the direction of the IUS) until 10 hours 45 minutes GET, when an attitude maneuver is performed to protect the payload bay from SRM-1 plume impingement. Fourteen minutes after SRM-1, the Orbiter maneuvers out of this protection attitude into a -ZLV attitude. A detailed separation time line is presented in table III .

Following SRM-1 and prior to deorbit preparations, the crew enters a quiesent period for which no major activities have presently been defined. IMU alinements are performed between the eat/sleep periods and, at 28 hours 30 minutes GET, the Orbiter maneuvers to the passive thermal control (PTC) attitude.

Preparation for deorbit begins at 40 hours 15 minutes GET. An IMU alinement is performed during the last darkness pass at 42 hours 45 minutes GET. The Orbiter maneuvers to the deorbit burn attitude at 44 hours 21 minutes GET and 5 minutes later, the deorbit maneuver is performed. The burn ΔV is 261 fps and the burn time is 135 seconds. The landing at KSC occurs at 45 hours 5 minutes GET (11:40 EST). The backup landing opportunity occurs at 46 hours 40 minutes GET (13:15 EST). The complete list of landing opportunities for the flight are found in table VII.

11.3 ORBITER ATTITUDE AND POINTING TIME LINE

The Orbiter conceptual attitude and pointing time line for Flight 7 is presented in table $\overline{\text{III}}$. This table contains the major attitude sequence of events and time line, the Orbiter orientation with respect to the instantaneous local

vertical/local horizontal (LVLH) reference, and the pointing angle necessary to orient the Orbiter longitudinal axis along the lines of sight to the Sun, Earth, and, if applicable, a second orbiting vehicle. The definitions of the pertinent angles are illustrated in figure 5.

Figure 6 illustrates the IUS and TDRS omni coverage assumed for the attitude time line definition. This coverage is expressed in terms of the allowable pitch/yaw envelope relative to the Orbiter body. Allowance was made (where data exist) for preliminary estimates of Orbiter body blockage, TDRS body blockage of the TDRS omni, and IUS/TDRS tilt table elevation effects.

Figure 7 presents pictorial summaries of the entire cnorbit phase of the Flight 7 mission. A detailed explanation of the program that drew these figures and a description of how to interpret each picture may be found on page 3 of reference 3.

4.4 SEPARATION TIME LINE

This separation sequence for TDRS-A is defined in reference 5. It is designed to satisfy all guidelines and constraints outlined in section 3. Table IV summarizes the IUS/TDRS-A separation sequence of events.

Separation is initiated at 10:05:00 GET when the IUS/TDRS-A is released from the tilt table. This corresponds to 00:00:00 phase elapsed time (PET), the reference time for all subsequent events. All Orbiter RCS jets are inhibited prior to release and remain inhibited for the first minute after release. Subsequent to one minute PET, only the +Z RCS jets are inhibited. They remain inhibited until the Orbiter window protection attitude maneuver is initiated 38 minutes after release. At 01:00 PET, a 4 second -X RCS burn is performed, followed by a 45-degree pitchdown maneuver. On completing the pitchdown maneuver at 1:49 PET, the Orbiter is placed in an inertial attitude bold with a 0.5 degree deadband. A 6-second -X RCS burn is then performed. At 10:00 PET, when the IUS/TDRS-A is about 1200 feet in front of and 400 feet above the Orbiter, the IUS attitude control system is activated. One minute later, at 11:00 PET, the Orbiter initiates a 35 second OMS burn. Figures 6(a) and 6(b) show the relative motion of the IUS with respect to the Orbiter during this portion of the separation sequence. Figure 6(c) also shows the payload interrogator (PI) antenna nominal beam width and contours of dynamic pressure caused by the OMS engines (from 11:00 through 11:35 PET). Five seconds after OMS burnout, at 11:40 PET, the attitude deadband is increased to 2 deg/axis and a 45-degree pitchup maneuver is initiated. At 12:27 PET, the pitchup maneuver is stopped and the Orbiter is maintained in inertial attitude hold. As shown in Figure 6(a), this ensures that the IUS/TDRS-A is visible through the overhead window and that the IUS remains within the nominal beam of the PI antenna. At 38:00 PET, the Orbiter +Z RCS jets are enabled and a maneuver to the window protection attitude is initiated. Six minutes later, at 44:00 PET, the Orbiter is at the desired attitude with the belly facing the IUS.

A LVLH attitude hold is initiated at this time in order to maintain this Orbiter-IUS relative attitude. Nominal IUS ignition occurs at 51:00 PET when as shown in Figure 6(d) the Orbiter is approximately 63 n. mi. behind and 36 n. mi.

above the IU.. Nominal IUS motor burn duration is 2 minuter 40 seconds (until 53:40 PET). At 65:00 PET, the IUS motor exhaust particles are sufficiently dispersed, and the Orbiter is free to maneuver out of its window protection attitude.

At the completion of the separation sequence, the maneuvers have consumed 110 pounds of forward tank and 65 pounds of aft tank RCS propellants and 1341 pounds of OMS propellant. The Orbiter is in an orbit with a 188-n. mi. apogee, a 150-n. mi. perigee, and an argument of perigee of +20 degrees.

4.5 NONPROPULSIVE CONSUMABLES

The nonpropulsive consumables loading for Flight 7 is shown in Table IX. The active thermal control system (ATCS) thermal profile is presented in figure 8 (a). The total source power profile is shown in figure 8 (b). Figures 8(c) through 8(e) present the scheduled venting time line for this flight.

4.6 PROPULSIVE CONSUMABLES

The OMS and RCS propellant budgets, along with the Orbiter mass properties time history, are presented in table X. The RCS propellant budget shown is the minimum RCS propellant usage for the mission. The OMS propellant budget shows the propellant usage for mission abort after the OMS-2 burn (case I) and the nominal mission (case II).

5.0 REFERENCES

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- 2. Shuttle Operational Data Book Revision A, Volume II, JSC-08934, Sept. 1975.
- 3. Presentation to Management Council, Orbiter Separation Requirements for Upper Stage Plume Avoidance, May 22, 1979.
- 4. E. Lineberry Separation Sequence review followup to Management Council briefing on Separation Sequence, May 31, 1979.
- 5. Wilson, W.S.: Orbiter/IUS Separation Sequence for Nominal TDRS-A Deployment. TRW Report 79:2511.1-61, May 17, 1979.

TABLE 1.- MAJOR EVENT TIME LINE FOR FLIGHT 7"
[Launch February 27, 1981 at 19:35 GMT]

Event	GET, hr:min:sec	Duration, hr:min:sec	Comments
Launch	00:00:00	00:08:10	Feb. 27, 1981 at 19:35 GMT
MECO	00:08:10		$h_a = 78 \text{ n. mi., } h_p = 12 \text{ n. mi.}$
ET separation	00:08:21		ΔV = 4 fps
OMS -1	00:10:10	00:02:11.0	$h_a = 150 \text{ n. mi., } h_p = 56 \text{ n. mi.,}$ $\Delta V = 211 \text{ fps}$
CMS-2	00:45:43.0	00:01:45.0	h _a = 150 n. mi., h _p = 150 n. mi., ov = 169 fps
Open PLED	01:20:00	00:05:00	
Transfer IUS To Orbiter power	01:30:00		
Perform IMU alinement	01:55:00	00:25:00	In darkness
Early predeployment checkout	02:25:00		
IUS command link check	02:52:30.0		HTS pass
TDRS RF command check	03:12:00	00:05:00	MIL pass
Orient Orbiter, perform IUS attitude initialization test	03:23:00	00:26:00	Backup TDRS RF command check (ACN) at 3:30
Downlink verification of IUS attitude data	04:14:30		GTS pass
Uplink SV and trim maneuver(s) to Orbiter	04:28:30		
Perform Orbiter trim maneuver(s)	04:57:00		RCS sequence, maximum of two maneuvers performed at apogee and/or perigee
IMU alinement	06:23:00	00:25:00	In darkness
Orient Orbiter, perform IUS attitude initialization	07:53:00		

5

5

TABLE I .- Concluded

Event	GET, hr:min:sec	Duration, hriminisec	Comments
Crew eat period	21:00:00	01:00:00.0	
IMU alinement	21:30:00	00:25:00.0	In darkness
In I alinement	27:45:00	00:25:00.0	In darkness
Orbiter maneuvers to passive thermal control attitude	28:30:00		RCS sequence .
Crew eat period	29:15:00	01:00:00.0	
Crew presleep activity	30:15:00	00:45:00.0	
Crew sleep period	31:00:00	07:15:00.0	
Crew postsleep activity	38:15:00	00:45:00.0	
Crew eat period	39:00:00	01:00:00.0	
Deorbit preparation	40:15:00		
IFU alinement	42:45:00	00:25:00.0	Last darkness pass
Close PLBD	43:15:00	•	
Orbiter maneuver to deorbit attitude	43:56:00		RCS sequence
Orbiter attitude adjustment maneuver	44:21:00		RCS sequence
Deorbit burn	44:26:00	00:02:24.0	$h_a = 173 \text{ n. mi., } h_p = 5 \text{ n. mi.}$ $\Delta V = 261 \text{ fps}$
KSC landing	45:05:00		
Backup KSC landing	45:40:00		

_

CASKY	65178#1	GETYSMT CCCCETIC			4111100 1.100441		LCCH ANGLES		LOCK ENSLES		A STATE OF THE STA		
	CAT HO MIN SEC	41 121	Lan	PITTE	7 4 %	ราเเ	rell	PIICH	FITCH	YA pi	HOUE	e E 1 4	5 U A
CMS-2 C.C. AND	01 0145143.0 55120123143.1	112.3 -27.5	79	-15:1	-17:7	193.5	-16.3	74.0	32.5	-31.6	1H	-31.6	•
MAN. TO HE LV	51127134117.3	151.4 -27.9	132.1	42.1	-11:5	160.0	-16.5	122.1	52.1 132.1	-31:7	ROIR	-31.7	1
CFEN PLan	0: 1:19:60.0 5x120:54:60.0	153.9 14.8	200.1	- *3.1	42.6	180.5	-146.7	73.0	-75.C 90.C	-31.7	LVLH	-31.7	1
MAN. TO CORS CAL	5512113711813	150.4 7.5	225.4	1.5.7	::1	190.9	-* 9 . S	142.1	158.2	-31:7	PTCG	-31.7	r
"AN. IC COFS CAL.	12: 1:54:40.7 5::21:30: •3		335.5	- f 6 • 1 1 • 1 • 7	-71:3	134.5	170.7	:5:5	-69.5 -11.5	15.5	16	-31.7	r
1-1 at 195. Mar. 70	57121154120.0	112.4 -29.6	53.5	1-11:5	-72:3	114.4	136:3	161.7	-72.C -13C.7	79.6 35.7	1н	-31.5	c
EA-LY PRE-PEPLOY.	2: 2:24:e0.7 5::22: 2: -3		94.7	-19.2	-51.9	120.1	-50.9	42.9	30.2 92.2	-31.8	LVLH	-31.8	r
SUNHISEPHE LV		151.6 +23.6	94.6	-21.5	-46.5	190.5	-62.9 0.	37.1	3:36	-31.8	LVLH	-31.8	•
103H2 2J4MMU2 2J17	0: 2:52:37.7 5::22:27:30.0		150.4	- 35. 1	57.4	180.C	-147.8 •0	61.2 90.5	-79.7 90.0	-31.8	LVLH	-31.6	1
ELFS RF COMMAND	0: 3:11:67.0 5::22:46:60.7	151.9 24.4	256.4	1.5.5	4 5 . 0	180.0	-121.5	141.7 90.0	-157.6 90.0	-31.5	LVLH	-31.8	1
SUNSCIVED UN	C: 3:22:29.0 55:22:57:39.3	150.4 5.0	384.9	152.6	£.6	180.C	-61.0 •3	30.5	159.8 90.0	-31.9 .3	LYLH	-31.9	C
MEN. TO CHAITCH 105 SCANNER	58:22:57:15:3	150.4 7.3	306.1	1 . 2 . 7	5:3	185.5	- « 9 . u	147.2	155.4	-31.3	ROTE	-31.9	. c
FACKER TERS PE	0: 7:30: .3 54:21: 4::0.3		329+1	-12.t	-56.6	-17.5	-157:4 -171:1	121.2	-133.5 -52.0	-16.9	1н	-31.9	r
HESTN CHEITEPITUS	L: 3:36:10.9		353.2	15.4	-of.5	-19.5	-157.4	131.3	-131.5 -100.0	-16.5	ROTR	-31.9	r.
FIRST TUE SCANNER	(1 3:37:12:0 Suiddildid	151.2 -19.5		16.2	-56.5 -23.4	-25.6	-151.4 -140.3		-135.C -101.4	-21.1 -39,7	ROTE	-31.9	r

ORIGINAL PAGE 19

TABLE II.- CONTINUED.

EVENT	GFT/GM1	5000011	c		HYBODY		LCCK		LCOK AN	RTH			
	CAY HP MIN SEC	ELT LAT	LON	PITCH	1 t n	POLL	CCLF	PITCH -	PITCH	YAN	MODE	BETA	SUF
INCOLIST HOLD	58123112124.7	111.7 -17.5	354.6	-147.5	-33:5	*11.t	-145.4	131.3	136:5	35:3	19	-31.9	r
CHAITER/ILE POLL	58127138140.3	151.6 -22.4	4.4	-147.2	-56.5 -23.4	·31.6	-145.4 -125.6	131.7	1-116.8	-25.3 -52.4	ROTE	-31.5	τ
SECOND ILS STANNER ON STAR I	5512 11511210	151.7 -22.6	5+2	-147.2	-16.5 -21.4	75.6	-151.9 -130.3	131.7	-135.2 -112.7	-21.1 -47.4	ROTE	-31.9	r
FIRST TUS "CANNER ON STAR 2	5812711812713	152.1 -25.0	16.1	+197.2	-56.5 -23.4	-170.2	111.0	131.3	-157.7	44.5 33.1	8019	-31.0	٦
INFELLATION BOTO	55123118139.3	152.1 -26.7	19.5	-147.2	-54.5	-164:3	105.C	131:3	-163.E	39:5	IH .	-31.9	r
- Ceclisaving Corr - 2 000 1250	5512719111117	1:2.3 -27.9	23.6	107.2	-56.5	78.0	105.1	131.3	-162.5	-16.5	RCTP	-31.0	r.
SUCCEND ILS SCANNER	50123146113.0	112.3 -27.0	20.6	-147.	-56.5 -27.4	-170.2	111.1	111.7	-157.7	22.3	ROTE	-31.0	·
ENE THE TOTAL RELE	51:27:21:24:0	152.3 -27.9	72.4	-147.2	-56.5 -23.4	-176.2	117:1	131.3	-152:6	16.2	FOTR	-31.9	,
THIRD IUS SCANNER ON STAR 1	55123124127.2	132.4 -28.6	43.5	-147.2	-56.5 -23.3	-25.6 92.2	-151.3 -93.4	131.3	-135.C	-21:1	ROTE	-31.9	Ċ
END ILS SCHNERA MAN. TO -Z LV	50:27:24:39:2	1:2.4 -29.6	44.4	-147.2	-56.5 -23.3	-31.6	-145.3 -86.5	131.3	-136.9 174.0	-25.3	HOTR	-31.9	c
	0: 1:53:60.0 58:23:26:60.0	152.2 -27.0	62.8	-18.1	-67.8	15C.0 1C1.1	- 47.7 • C	45.6 90.0	34.6 9C.C	-31.9	L YL H	-31.9	c
SUMPISENTS LV	5::27:32:37:0	151.7 -23.6	77.5	-22.1	-46.6	190.0	-61.1 •3	37.1 *C.C	20.1 90.6	-31.9	LVLH	-31.9	1
TELLAND .	57: 0: 3::0:0	157.1 26.5	199.1	-52.6	77.5	160.5 115.4	-147.1	103.0	-105.4 90.0	-31.9	LVLH	-31.9	,1
FLEFORY TRIM MAN. IF PLICITED	G: 4:56:60.0 54: 0:31:60.0	110.34	205.5	151.5	-10.5	190.0	-45.7	132.4	142.7	-32.2	TAFH	-32.0	r
\$1858 17-7 14	5v: 1:57:49.2	150.4 7.4	3.393	152.7	æ:	150.0 -95.1	-c1.1	142.6	159.7 96.0	-32.1	LVLH	-32.1	۲.

Fift	651/641	SECTETIC	#1111UF E #E#750		LOGE ANCLES	ECCH ANGLES SUNVEARTH			
*****	LAY HO MIN SEC PLT	LAT LON	PITCH Y	in soli	FCLL PITCH	FIICH TAN	⇒or €	EET#	50*
was a TO ING ALINE	: (:2%:00.7 1'D.	2 3.2 267	141:5	-130.0	-52.5 137.5 -0.0 40.5		Troir •	- 22 - 1	. r
140 15151	Sv: 4:77:55 -7 150.	-2,5 277.0		112.5	1:7.3 35.2	*69.1 80.4 *23.1 27.2	IH ·	-32 - 1	•
fnc #1111/10 -2 1 v	6: 6:45: +C 152+	5 -2713 - 33412		7.4 45'.e 6.3 171.9	99.0 e6.6 132.1 123.1	-69.0 80.4 -109.1 46.3	4019	7 . Sc -	٤
\$69(15f7+2) CV	-: 4:57:42.7 151. 57: 7:32:42.7	7 -21.1 12.5	-72.7 -49	147:7	-61.1 37.4 10 10.0	₹8:£ -32:5	FAC	-32+2	•
SCHOOLIVERS TO CONTINUESCAUSER	1: 7:52:10.7 150. 59: 7:27:50.0	7.1 237.5	172.6	140.6	-61.2 142.5 2.09	159.7 -32.3	FGTR	-32.3	ŗ
THE ETTING CONTINEY	1: 4: 5: 40 1'0. *y: 1:3%:60:0	4 -4,4 240,5	-147:: -5	-20.6	-157.3 151.4 -170.7 42.4	-113.1 -16.9	1н -	-32.3	C
-0.1% TOT SCENNER CN TITHIROLL 45	.: 4: 1:60.5 142. 5:1 7:16:60.0	K -15+1 267+5	-141.		-157.4 131.7 -164.3 -6.7	-133.1 -16.5 -56.6 -15.7	FC15	- 32 - 3	•
FIRST TO STRAKER	501 7131112.5 1:Co	E +10+5 - 25+++	-147.4 -2	111 7615	-1:1.4 1:1.7 -1:7.6 57.2	-135.C -21.1 -86.9 -22.3	P010	- 37 - 3	•
eter warentheattal	- 1 51 71 4 C 110 .	6 -11.5 255.5	-147.2 -2		-145.4 131.3 -151.3 27.6	-176.9 -25.3	in ·	-32.3	ŗ
CHITEFAILS BOLL	541 114167.0 111.			3.4 -32.6	-145.3 131.3	-136.9 -25.3 -94.3 -37.6	FOIR	- 32 - 3	
SECOND TUS SCANNER	0: 8: 5:10.0 151. 55: 7:40:12.0	0 +15.7 276.5	6.9 -5	6.2 -26.6	-151.3 131.3 -147.7 93.8	-135.C -21.1 -94.5 -32.3	PCIR ·	-37.2	ŗ
FIRST TUE SCANNER	51 \$1 614747 151. 5+1 7:4214742	5 -2016 / 29,14	-147.2 -5	176.3	111.2 151.4 175.9 161.0		ROTE	- 32 • 2	ç
SIDE MANAZONERTIAL	1: *: \$: 10.7 151. 5:: *:#3::5:7	-25.9 291.1	26.6 -51 -147.2 -2	6.2 76.3	105.2 131.4	-163.4 46.4 -111.6 57.5	IH	-32.2	÷
CASTLEY ILS FOLL	0: 5:11:20:0 157. 19: 1:40:20:0			76.9	105.2 221.7	-163.4 #6.4 -115.5 ##.5	E 6 12	-52.2	٢
SECOND TES SCANNER	6: *:1::12:9 142. 5:: *:47:12:5	0 -25.1 305.0	14.4 -5	70.3	111.2 131.3	-157.7 49.4 -115.9 35.3	ROIR	-32.2	ŧ

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EVENT	SETVENT	SECRETIC	1757774 17067444	LOOK ANGLES	LUCK ANGLES SUN/EARTH	
	LEAR HE HIN SEC. A	LT LAT LON	FITCH YEA FOLL	POLL PITCH	PITCH YAN	MODE BETA SUN
END TUR SCHANGE	ev: 4:12:44.0 15	2.h -25.8 30.46	-147.2 -54.2 -64.9		-152.5 41.9 -112.5 32.3	FC1F -32.2
THIRD FOR SCANNER	571 511511716 1"	2.3 -27.6 21:49	44.1 -54.2 -26.7 -147.4 -27.4 92.2		-135.2 -21.2 -142.2 -55.5	HOTP -32.3 C
END ILS SCANNEDA -	2: F:15:19:2 11 59: 1:50:19:2	2.7 -27.7 217.2	48.8 -56.2 -32.7 -147.2 -23.4 46.2		-137.C -25.4 -152.6 -61.9	ROTR -32.3 C
*. LV	0: #:19::0:0 15 %9: %:5%:60:0	2.4 -22.5 357.0	-7.2 -76.7 111.1		51.4 -32.3	LACH -35.3
INS CHECKGLE AND		3.3 -0.7 47.1	0.081 C	-114.2 35.0 00.0	-16.6 -32.3 9C.C .C	IH -32+3 1
MAN. TO TEPLOYMEN		n.	-12.2 47.2 96.3		-66.1 -17.1 95.5 -17.1	FCIP -32.3 1
DEFLOYMENT ATT.	. 0: 2:52:60.0 11 5-: 4:27:10.0	1.7 20.1 / 97.2	-109.3 51.1 -170.7	179.9 127.5	-122.5 -31.5	IH -32+3 1
		2.9 20.5 141.5	-109.0 51.1 -175.8	179.9 162.5 -9.1 105.9	-126-6 -3:3	1H -37+2 1
TURS HE CHECKOUT	59: 4:15: .7 15 59: 4:49:66.7	1.4 20.2 187.1	-100.1 51.2 -170.6	180.0 122.1	-122:1 137:6 15:7	1H -32.4 1
ELEVATE TABLE TO	2: 9:57:60:0 i'	1.5 -22.8 344.2	-128.9 -33.9 -159.9 -178.9 51.2 -170.9	180.0 171.9	-121.9 -48.8 -11.0	1H -32.4 1
פנינסיינאד לשנכד.	0:10: 4:60.0 15 54: 5:39:60.0	0.4 -17.1 13.6	-173.9 -37.9 -159.9 -176.9 51.1 -170.6		-121.9 -24.2 -26.7	14 -32.4 1
1 -1 114 11 - x 805	E:10: 5:60.0 15 59: 5:40:62.0	7.7 -17.4 17.0	-56.6 -37.7 -159.5 -108.5 51.2 -171.2		-121.61 -19.9 -28.5	IH -32.4 1
CHAITER PITCH DON MANAZIVENTIAL	4 Lil?: 6:49.1 1.	0.0 -9.9 19.6	-10.5 -10.7 -142.7 -45.6 3*.3 141.9	-179.9 76.6 -50.4 40.5	-76.6 28.5 -30.0	RCTR -32.4 1
165 905 701194710	. d:10:15: .0 15	3.1 F.7 46.7	-18.1 -10.9 -142.7 -45.6 38.3 141.9	-179.9 76.6 -+C.3 72.7	-76.6 67.1 -39.5	ROTE -32.4 1
INTITUTE OF SEP.	10110115160.0 15 148 5:51: 40	0.2 0.5 52.0	*14.1 -10.9 -142.7 -45.6 38.3 141.9		-38.6	ROTE -32.4 1

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EVENT	GET/CHT	61,001,110		41111UPC Late/60: 1		LCCH ANGLES		LOOK ANCLES SUNVERETH					
	INT HO HIM SEC 4	Li LAT	CON	PITCH	7.4 m	-011	rail	PITCH	FIICH	74.	-0°E	FETA	511*
TERMINETT CHS		2.4	5	-11.7 -45.6	-;(:;	-142.7	-179.9 -19.5	76 + 6 78 + 5	-7t -t 15 - 7	-39.6	14	-32.4	1
INTITATE PITCH UP	5:10:16:47:3 15 59: 5:51:47:3	5.4 S.F	52.3	-11.7	-12:3	-142.7	-1*C.C	16.9 18.5	-76.4 75.2	-33:3	4578	-32.4	1
THERTIPL HOLD	C:10:17:27:9 15: 5:: 5:52:47:7	5.11	54.6	- 1 3 · 1 - 1 1 1 · 7		-161-1	-179.9	123.7 46.7	-121.7	-23.4	IH	-32.4	3
PRUT. ATT./ORE	6:10:42:00:0 17 55: 6:16: -7	5.8 22.5	15000	153.5	-1::5	145.5	-100.7 -180.0	117:1	-117.6	-32.5	FOTP	-32.5	1
15ERTIFE HOLDVIUS	0:10:55:40+3 le 59: 6:30:40+3	5.t 1.4	201.:	153.6	3::i	147.5	-1+3.1 -1#0.0	117.C	-56 · 1 -117 · C	-32.5	114	-32.5	r
········	59: 8:45: • 15:	6.5 -27.7	24:00	114.5	-6013	182.5	-12.6	¥0.5	95.0	-37.5	LVLH	-32.5	ŗ
meeth deve	1:13: 9:60.3 15 55. 8:45: .0	3.7 -5.3	374.7	-27.0	.;;?	165.C	-120.2	38.7	-21.9 96.6	-32.7	FAFH	-37.7	1
ENC SLEEP/+2 LV	5,:120:15: .0 le	6.7 -23.7	114.4	1 40.1	-67.4	110.0	-73.2	5.70	92.6 92.0	-32.2	LVLM	-33.7	r,
MAN. TO THE ALTHE.	55117124167.7 15	1.9 31.7	21.4	152.0	16.3	195.0	-81.6	146.1	174.4 96.0	-31.3	ROTE	-33.2	1
140 40 MT.	L:21:30: +0 15	5.7 2.1	31.7	-60.7	-69:3	47.2 129.2	99.5 132.8	66.7 21.3	-75.6 -14.8	80.0 15.5	1H	-37.3	r
ENC IME ALTHE . / MAN. TO +2 L.	54:17:145: •0 15 54:17:14:e0•3	7.2 -23.0	4.6A	-9.8	-69.3	129.C	99.5	46.6 80.2	-16.4 -75.7	79.9	ROTR	-33.3	t
-2 LV	54:17:34:00.0 17	2.84-1.5	124.6	-11.6	- 6C - 5	106.9	-38.2	62.5 90.0	56.5	-33.3	IH	-33.3	τ
THE ALINE.	1: 7:45: .7 16 54:27:14::7.7	5.5 -19.7	343.6	-21.3	-65.2	45.5 129.5	99.6	86.9	-72.5	ec.o 42.5	111	-33.6	ŗ
END INC ALTHERA	1: 4:15:00.0 15		114.9	117.E	-69.1	46.9 129.1	99.5	67.0 152.4	-72.t	80.0 -19.1	FOIF	-33.7	1
HEGIN DICKROLL +3	1: 4:36: .9 15 5u: 5: 4:60-5	1.6 19.3	154.2	73.0		70.C	156.3	89.6 121.6	89 · f -124 · 1	20.5	ROTR	-33.7	ı

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TABLE II .- CONCLUDED.

£ v5 % T	6F1/6#1	95006710	FITTIUDE EXEMPECET	LOOP ANGLES	LOCK ANGLES	
	CAN HE MIN SEC.	ret ett ten	PTICH YEA FOLL	POLL FIICH	PITCH YAL	MODE BETA SUN
PESIN TELLE		11.9 -29.2 35	-55.1 -55.7 90.6 -86.1 -14.2 -18.4	79.5 69.6	89.54 56.5 34.4	ROTE -33.8 C
- t % - SUEU F	1:14:15: .º 1 6:: 9:47:00:	·*·* •12•7 149•0	-177.1 -55.3 -57.7 -66.1 -14.2 161.6	179.9 +9.E 135.1 63.0	-99.5 -54.2 39.0	801F -34.2 F
TAL PICZMAN. TO	1:14: 1: .7 1	-3.5 -20.9 200.7	-75.6 -55.2 92.7 -56.1 -14.1 -18.3	1 89.5 23.3 57.4	89.51 55.7 17.0	ROTE -34.3 C
CLUSTIT OHIRAN	1:16:15: 20:1	13.0 -15.6 250.6	144.3 -65.2 129.2		-75.0 87.1 -170.7 13.2	IH -34.3 1
INC ALIME	1:15:45: .7 1 6::14:19:5: .8	7.0 -0.4 93.2	144.3 -69.3 129.3	137.4 40.0	-75.1 ts.1	IH -34.4 C
FURTE FURT	1:19:15: .7 1	5.4 -10.4 204.4	45.2 7.7 45.1 144.2 -65.3 129.3	99.5 47.5 126.5 158.0		IH -34.5 1

GET, PET, nr:min:sec min:sec		Event	Remarks		
10:05:00	0:00	Release IUS from tilt table	AV = 0.40 fps; IUS +X axis pointed 180° away from Sun; Orbiter pitch/yaw/roll = -100.90°/-33.90°/ 200.00°; RCS inactive		
	1:00	Begin 4-second -X RCS burn	PRCS with +Z jets inhibited		
	1:04	End -X burn; begin 45° Orbiter	$\Delta V = 1.1$ fps; accelerate to $-1.0^{\circ}/$ sec pitch rate		
	1:49	End pitch-down maneuver; initiate Orbiter inertial hold; begin 6-sec -X RCS burn	Deadband = 0.5°/axis		
	1:55	End -X burn	$\Delta V = 1.7 \text{ fps}$		
	10:00	IUS attitude control system activation	Orbiter-IUS range = 1306 ft; IUS -X axis pointed r 140 away from Sun, due to gravity gradient and aero torques		
10: 16: 00	11:00	Begin 35-second OMS burn	Orbiter pitch/yaw/roll = -14.07°/ -10.87°/217.27°		
•	11:35	End OMS burn	$\Delta V = 67.6 \text{ fps; } h_A = 188 \text{ n. mi., } h_p = 150 \text{ n. mi., argument of erigee} = 20^{\circ}$.		
•	11:40	Begin 45° Orbiter pitch up maneuver	Accelerate to +1.0°/sec pitch rate		
	12:27	End pitch-up maneuver; initiate Orbiter inertial hold	Deadband = 2.0°/axis; IUS visible through overhead window		
	34:00	Orbiter-IUS range = 20 n. mi.	Max RF communication distance		
10:43:00	38:00	Orbiter begins maneuvering to window-protection attitude	Enable +Z jets		

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TABLE III.- Concluded

GET, hr:min:sec	PET, min:sec	Event	Remarks		
	44:00	Orbiter achieves window- protection attitude; begins LVLH attitude hold	Orbiter pitch'yaw/roll = -177°/ 0°/180°		
	45:00	IUS SRM ordinance enable			
	45:22	Orbital sunset			
10:56:00	51:00	Nominal IUS SRM-1 ignition; Orbiter begins inertial nold	IUS in inertial hold @ roll/pitch/ yaw = -119°/12°/0° wrt local vertical		
	53:40	Nominal IUS SRM-1 burnout			
11:10:00	65:00	Orbiter free to maneuver out of window-protection attitude			

TABLE IV .- FLIGHT 7 WEIGHTS AND CENTERS OF GRAVITY DATA

Component	Wt, 1b	X _{cg} , in.	Yog, in.	Z _{cg} , in.
Orbiter dry weight	169 242.0	1106.1	0.1	369.6
Nonpropulsive consumables	5 165.6	917.5	-6.1	351.3
MPS propulsive	5 206.0	1406.7	6.4	353.9
OMS propulsive	17 700.0	1429.1	0.0	476.2
RCS propulsive	5 361.0	1040.0	1.5	438.9
Payload	49 234.0	1053.1	-1.6	394.9

TABLE V.- ASSUMED COMMUNICATIONS NETWORK AVAILABLE TO SUPPORT FLIGHT 7 (FEBRUARY 27, 1981)

(a) GSTDN

Station	Geodetic latitude positive N, deg	Longitude positive E, deg	Altitude, ft
ACN	-7.90	345.67	1 743
BDA	32.18	295.34	-111
Goldstone (GDS)	35.16	243.13	3 014
ETC	39.00	283.16	- 7
G WM	13.22	144.74	381
Kwajalein Island (K9A) (C-band)	9.40	167.48	37
ΗΛW	21.99	200.35	3 739
MAD	40.27	355.83	2 650
Merritt Island (MIL)	28.35	279.22	-178
Orroral (ORR)	- 35.45	148.98	3 039
QUI	-0.62	281.42	11 640
A GO	- 32.98	289.33	2 318
Fairbanks, Alaska (ULA)	64.83	212.48	

TABLE V .- Concluded

(b) AFSCF

•				
Station	Geodetic latitude positive N, deg	Longitude positive E, deg	Altitude, ft	
Cape (TEL-4)	28.35	279.31	48	
Guam (GTS)	13.61	144.85	528	
HTS	21.57	201.74	942	
ios	-4.67	55.48	1936	
New Hampshire	42.52	288.37	692	
Thule (TTS)	76.52	291.48	466	
Vandenberg (VTS)	34.82	239.50	1001	

TABLE VI.- FLIGHT 7 STATION CONTACT OPPORTUNITIES FOR COMMUNICATIONS AND NAVIGATION

(a) GSTDN network coverage for nominal flight [OMS-2 through deorbit]

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev.,	Min. slant range, n. mi.
ACN	00:01:55:27	00:02:02:19	6:52	25	331
KMRa	00:02:43:23	00:02:50:44	7:21	82	152
HAW	00:02:52:23	00:02:59:43	7:20	60	174
GDS	00:03:03:03	00:03:09:01	5:58	16	467
WHSb	00:03:05:09	00:03:11:59	6:50	22	369
MIL	00:03:11:26	00:03:17:36	6:10	14	505
ACN	00:03:31:17	00:03:37:25	6:08		· • .
GWM	00:04:13:57	00:04:21:08	7:11	39	233
KMR	00:04:19:55	00:04:24:58	5:03	8	644
HAW	00:04:28:10	00:04:34:54	6:44	20	385
GDS	00:04:38:41	00:04:43:07	4:26	8	668
WHS	00:04:41:00	00:04:45:52	4:41	8	672
QUI	00:04:50:12	00:04:56:36	6:25	17	432
GWM	00:05:49:35	00:05:56:04	6:29	17	438
HAW	00:06:03:47	00:06:10:32	6:45	20	380
QUI	00:06:25:11	00:06:32:01	6:50	24	338
103	00:07:02:10	00:07:08:00	5:50	12	539
GWM	00:07:27:20	00:07:29:48	2:28	4	817
HAW	00:07:38:57	00:07:46:18	7:21	63	168

 $^{^{\}rm a}{\rm Kwajalein}$ Island C-band; used for tracking support. $^{\rm b}{\rm White}$ Sands; included for information.

TABLE VI .- Continued

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev. deg	, Min. slant range, n. mi.
AGO	00:08:09:31	00:08:09:45	0:13	6	756
105	00:08:36:44	00:08:43:56	7:12	41	224
HAW	00:09:14:33	00:09:20:58	6:25	16	449
A GO	00:09:41:41	00:09:46:24	4:42	18	426
GWM	00:10:38:29	00: 10:43:13	4:44		
KMR	00:10:43:34	00:10:50:25	6:50	15	557
A GO	00:11:17:01	00:11:22:38	5:37	29	340
ACN	00:11:31:32	00:11:38:26	6:54	21	387
GWM	00:12:13:24	00:12:21:13	7:48	29	348
KMR	00:12:18:58	00:12:27:17	8:19	60	212
AGO	00:12:53:13	00:12:58:14	5:01	18	467
ACN	00:13:07:32	00:13:14:24	6:52	22	364
GWM	00:13:49:24	00:13:57:16	7: 52	26	380
KMn	00:13:56:47	00:14:01:24	4: 36	6	842
AGO	00:14:30:23	00:14:31:33	1:10	5	825
QUI	00:16:06:52	00:16:11:33	4:40	7	688
QUI	00:17:41:34	00:17:48:53	7:19	75	154
MAD	00:18:03:30	00:18:07:42	4:12	6	767
ORR	00:18:44:18	00:18:49:28	5:09	14	591
QUI	00:19:19:25	00:19:23:08	3:43	- 5	749
MIL	00:19:23:34	00:19:24:48	1:14	. 3	857
BDA	00:19:25:47	00:19:26:28	0:42	5	787

TABLE VI.- Continued

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time,	Max elev., deg	Min. slant range, n. mi.
BDA	00:19:26:55	00:19:30:12	3:17	7	716
MAD	00:19:38:59	00:19:42:57	3:57	6	809
IOS	00:19:55:33	00:20:02:35	7:03	15	556
ORR	00:20:19:56	00:20:25:37	5:41	19	477
MIL	00:20:56:22	00:21:03:14	6:51	21	381
BDA	00:21:00:08	00:21:07:05	6:58	21	387
IOS	00:21:30:55	00:21:39:14	8: 19	43	267
ORR	00:21:55:60	00:21:59:34	3:34	12	595
WHS	00:22:27:37	00:22:32:47	5:11	9	645
MIL	00:22:31:53	00:22:39:29	7:36	70	169
ETC	00:22:34:19	00:22:39:24	5:04	8	692
BDA	00:22:35:40	00:22:43:09	7:29	32	292
IOS	00:23:09:07	00:23:13:34	4:27	6	851
HAW	00:23:51:53	00:23:54:57	3:03	5	768
GDS	01:00:01:08	01:00:05:59	4:51	10	616
WHS	01:00:02:19	01:00:09:24	7:05	24	358
MIL	01:00:07:50	01:00:15:38	7:48	82	167
ETC	01:00:09:41	01:00:14:55	5:14	.8	703
BDA	01:00:11:36	01:00:18:49	7:14	21	421
ACN	J1:00:28:30	01:00:29:10	0:40	5	879
ACN	01:00:29:44	01:00:34:12	4:28	9	733
KMR	01:01:16:41	01:01:23:21	6:39	19	398

TABLE VI .- Continued

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi.
	01:01:25:22	01:01:32:37	7:14	41	225
HAW	\	01:01:42:16	6:10	17	458
GDS	01:01:36:05	01:01:45:23	7:27	31	306
WHS	01:01: 7:56		6:50	32	307
MIL	01:01:44:42	01:01:51:32		. 3	942
ETC	01:01:47:13	01:01:47:13	0:53	7	783
BDA	01:01:48:25	01:01:52:01	3:35		783
BDA	01:01:52:26	01:01:53:12	0:46	7	
ACN	01:02:03:06	01:02:11:34	8:28	88	188
	01:02:48:30	01:02:54:04	5:34	11	577
GWM	01:02:48:37	01:02:54:05	5:28	10	589
GTS	•	01:02:59:25	6:53	23	343
KMR	01:02:52:33	01:03:08:40	7:13	31	283
WAH	01:03:01:26		6:17	14	534
GDS	01:03:11:46	01:03:18:02		17	480
WHS	01:03:13:57	01:03:20:54	6:58	8	728
MIL	01:03:20:40	01:03:26:08	5:28		799
QUI	01:03:24:53	01:03:29:29	4:36	7	
ACN	01:03:40:18	01:03:46:45	6:27		
	01:04:23:31	01:04:30:49	7:18		~ →
GWM	a. 00.51.25	01:04:33:06	1:32.	3	853
KMR	04.07.57	- h hh . F.C		19	420
WAH				5	836
GDS				14	863
WHS	01:04:51:22	2. 01.0			

TABLE VI .- Continued

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi.
QUI	01:04:59:10	01:05:07:28	8:18	64	203
IOS	01:05:38:52	01:05:41:11	2:19	4	860
GWM	01:06:00:49	01:06:06:00	5:11	9	637
— HAW ···	01:06:14:00	01:06:21:34	7:34	31	.306
QUI	01:06:36:07	01:06:42:36	6:29	12	649
IOS	01:07:12:36	01:07:19:53	7:17	35	260
HTS	01:07:50:16	01:07:58:17	8:01	52	220
AGO	01:08:17:43	01:08:19:30	1:47	11	660
AGO	01:08:20:35	01:08:23:04	2:29	14	586
108	01:08:49:11	01:08:55:13	6:02	13	522
GWM	01:09:16:51	01:09:17:48	0:57	3	893
KMR	01:09:21:22	01:09:25:23	4:02	6	ô17
WAH	01:09:26:58	01:09:32:26	5:28	8	738
A GO	01:09:53:32	01:09:59:21	5:48	28	366
ACN	01:10:08:55	01:10:10:10	1:15	6	761
ACN.	01:10:10:30	01:10:14:50	3:34	8	684
GWM	01:10:50:35	01:10:56:57	6:22	12	587
KMR	01:10:55:46	C1:11:03:42	7:56	31	303
AGO	01:11:29:41	01:11:35:13	5:32	26	373
ACN	01:11:43:54	01:11:51:25	7:32	74	162
GWM	01:12:25:54	01:12:34:06	8:12	84	180
KMR	01:12:31:60	01:12:39:27	7:27	19	481

TABLE VI.- Continued

(a)	Concl	uded
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Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi.
AGO	01:13:06:07	01:13:08:24	2:17	12	610
AGO	01:13:09:51	01: 13: 10: 13	0:22	12	610
AGO	01:13:10:19	01:13:10:33	0:14	5	811
ACN	01:13:21:27	01:13:10:33	3:34	7	685
ACN	01:13:25:40	01:13:25:57	0:17	3	862
G <i>W</i> M	01:14:02:51	01:14:08:58	6:07	10	688
QUI	01:16:18:29	01:16:25:18	6:49	21	372
MAD	01:16:18:29	01:16:43:58	2:28	т 4	836
QUI	01:17:54:33	01:18:01:09	6:36	19	400
MAD	01:18:15:47	01:18:20:08	4:21	6	757
108	01:18:34:17	01:18:36:55	2:38	4	911
ORR	01:18:56:45	01:19:02:25	5:40	17	510
MIL	01:19:33:55	01:19:39:18	5:23	10	605
BDA	01:19:37:03	01:19:43:26	6:02	13	530
MAD	01:19:52:29	01:19:53:41	1:12	, 3	904
ORR	01:20:32:35	01:20:37:55	5:30	17	505

TABLE VI .- Continued

(b) AFSCF RTS coverage [OMS-2 through 24 hours in parking orbit]

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi.
HTS	00:02:52:42	00:02:59:59	7:17	45	210
VTS	00:03:02:09	00:03:08:46	6:36	18	426
TEL-4	00:03:11:26	00:03:17:38	6:12	14	497
GTS	00:04:14:01	00:04:21:11	7:10	37	244
HTS	00:04:28:34	00:04:35:09	6:34	18	425
VTS	00:04:37:31	00:04:43:07	5:35	10	594
GTS	00:05:49:36	00:05:56:10	6:33	18	424
HTS	00:06:04:11	00:06:10:51	6:40	19	404
IOS	00:07:02:10	00:07:08:00	5:50	12	539
GTS	00:07:27:11	00:07:30:02	2:51	. 4	801
HTS	00:07:39:19	00:07:46:40	7:21	62.	171
IOS	00:08:36:44	00:08:43:56	7:12	41	224
HTS	00:09:14:56	00:09:21:20	6:24	16	457
GTS	00:10:38:23	00:10:43:20	4:58		••
GTS	00:12:13:22	00:12:21:14	7:51	30	332
GTS	00:13:49:25	00:13:57:14	7:48	25	397
TEL-4	00:19:23:22	00:19:24:58	1:37	3	849
IOS .	00:19:55:33	00:20:02:35	7:03	15	55€
TEL-4	00:20:56:21	00:21:03:14	6:53	22	373
IOS	00:21:30:55	00:21:39:14	8: 19	43	267
TEL-4	00:22:31:53	00:22:39:29	7:36	73	165

TABLE VI .- Concluded

(b) · Concluded

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi.
	00:22:37:40	00:22:38:18	0:38	3	910
ios	00:22:31:10	00:23:13:34	4:27	6	851
HTS	00:23:51:17	00:23:55:40	4:23	7	702
VTS	01:00:00:18	01:00:05:41	5:23	9	633
TEL-4	01:00:07:50	01:00:15:38	7:48	86	166

TABLE VI.- Continued

(c) GSTDN coverage for alternate deployment opportunities

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi
ACN	00:01:55:27	00:02:02:19	6:52	25	331
KMR	00:02:43:23	00:02:50:44	7:21	82	152
WAH	00:02:52:23	00:02:59:43	7:20	60	174
GDS	00:03:03:03	00:03:09:01	5:58	16	467
WHS	00:03:05:09	00:03:11:52	6:50	22	369
MIL	00:03:11:26	00:03:17:36	6:10	14	505
ACN	00:03:31:17	00:03:37:25	6:08		
GWM	00:04:13:57	ro:04:21:08	7:11	39	233
KMR	00:04:19:55	00:04:24:58	5:03	8	644
HAW	00:04:28:10	00:04:34:54	6:44	20	385
GDS	00:04:38:41	00:04:43:07	4:26	8	668
WHS	00:04:41:00	00:04:45:52	4:41	. 8	672
QUI	00:04:50:12	00:04:56:36	6:25	17	432
GWM	00:05:49:35	00:05:56:04	6:29	17	438
HAW	00:06:03:47	00:06:10:32	6:45	20	380
QUI	00:06:25:11	00:06:32:01	6:50	24	338
GWM	00:07:27:20	00:07:29:48	2:28	4	817
HAW	00:07:38:57	00:07:46:18	7:21	63	168
A GO	00:08:09:31	00:08:09:45	0:13	6	756
WAH	00.09:14:33	00:09:20:58	6:25	16	449
AGO	00:09:41:41	00:09:46:24	4:42	18	42€

TABLE VI.- Continued

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev, deg	, Min. slant range, n. mi
GWM	00:10:38:51	00:10:39:48	0:57	5	785
GWM	00:10:40:08	00:10:42:37	2:28	_ 6	750
KMR	00:10:43:52	00:10:49:44	5:52	12	536
AGO	00:11:16:42	00:1/1:21:40	4:58	25	334
ACN	00:11:30:54	00:11:37:36	6:42	20	381
GWM	00:12:12:54	00: 12: 19:50	6:56	25	329
KMR	00:12:18:28	00: 12:25:46	7:18	54	184
AGO	00:12:52:01	00: 12:56:38	4:37	15	466
ACN	00:13:06:04	00:13:12:52	6:48	22	357
G <i>W</i> M	00:13:48:11	00:13:55:00	6:50	22	360
KMR	00:13:56:03	00:13:58:30	2:27	4	823
A GO	00:14:28:32	00:14:29:15	0:43	4	823
QUI	00:16:04:03	00:16:08:21	4:18	7	697
QUI	00:17:37:49	00:17:45:06	7:17	83	149
MAD	00:18:00:04	00:18:03:37	3:33	5	774
ORR	00:18:40:38	00:18:42:03	1:25	8	664
ORR	00:18:44:06	00:18:44:06	0:20	9	633
QUI .	00:19:14:42	00:19:18:47	4:05	6	721
BDA	00:19:21:26	00:19:21:51	0:25	4	818
BDA	00:19:22:25	00:19:25:28	3:03	6	736
MAD	00:19:34:53	00:19:37:48	2:55	.5	80ύ
108	00: 19:51:27	00:19:57:04	5:37	11	568

TABLE VI.- Concluded

(c) Concluded

Station ID	GET AOS, day:hr:min:sec	GET LOS, day:hr:min:sec	Tracking time, min:sec	Max elev., deg	Min. slant range, n. mi.
ORR	60:20:15:24	00:20:19:56	4:33	15	474
MIL	00:20:51:10	00:20:57:50	6:40	19	400
BOA	00:20:54:57	00:21:01:39	6:42	19	399
ORR	00:21:50:36	00:21:53:22	2:46	11	583
WHS	00:22:21:45	00:22:26:34	4:49	8	669
MIL	00:22:25:55	00:22:33:18	7:23	63	169
ETC	00:22:28:31	00:22:33:05	4:34	7	702
	00:22:29:46	00:22:36:52	7:07	30	291
BDA	00:22:25:10	00:23:47:45	2:35	ц	813
WAH	00:23:54:35	00:23:59:01	4:26	9	638
GDS	00:23:55:38	01:00:02:26	6:49	21	371
WHS	01:00:01:23	01:00:08:34	7:11	80	154
MIL		01:00:07:47	4:37	7	699
ETC	01:00:03:10	01:00:11:41	6:42	19	407
BDA	01:00:04:59	01:00:26:02	3: 13	5	760
ACN	01:00:22:49	01:00:20:02			

TABLE VII.- FLIGHT 7 LANDING OPPORTUNITIES FOR FEBRUARY 27, 1981 AT 19:35:00

NAME • KSC	LAT=	28.615	LONG= -80.695	RADIUS =	3441.	
ORBIT	XRNG	TASR	TESS	GETL	LLT	SELV
1 A 2 D 3 D 14 A 15 A 16 A 17 D 18 D 19 D 30 A 31 A 32 D 34 D 35 A 46 A	-1. -117. -471. -858. -361. -64. -13. -218. -644. -662. -230. -16. -58. -347. -838. -487. -126.	7 58 9 33 11 8 3 15 4 56 8 35 11 10 3 17 4 52 8 27 8 27 11 11 3 18 4 53	3 32 1 57 0 22 8 16 6 41 5 32 1 22 8 42 7 32 8 47 8 47 8 47 8 47 9 27 9 27 9 42	0 0 14 0 1 49 0 3 25 0 19 30 0 21 50 1 0 15 1 1 50 1 22 40 2 15 1 22 40 2 0 15 2 1 51 2 2 30 2 21 5	14 49 16 24 17 60 10 5 11 40 13 15 14 50 16 25 18 0 10 5 11 40 13 15 14 50 16 26 18 0 10 5 11 40	426703366713366831 426703513366331
48 D 800 *STACN	-1. .F7RAD :	6 28	5 7	2 22 41	13 16	54.

OR POOR OR PAGE

TABLE VIII. - FLIGHT 7 SUNRISE/SUNSET DATA

	GETS =	0: 0: 0	GETF 46:40: 0	UECFIL /FILEO	LULH LULM
111111	TERMIN SET EFF SUNSET OND SUNSET MIDMIGHT OND SUNDISE EFF SUNDISE TERMIN RISE ONDIT NOON	GET D H H S 0 -1-12-35 0 -1 -7-36 0 -1 -7-35 0 0-50-4 0 0-32-32 0 0-27-35 0 0-5	2 27 10 22 24 17.4 2 27 18 27 24 8.8 2 27 18 27 24 8.3 2 27 18 44 55 -21.8 2 27 19 2 27 -23.9 2 27 19 7 25 -17.3	-5.0 151.6 150.9 12.3 150.9 72.2 148.7 145.0 149.6 145.0 148.6 163.8 149.1	PITCN YAU 100.0 21.4 -100.0 31.5 -100.0 31.5 -50.0 31.5 -19.8 31.5 -19.8 31.5 -0 31.5
ឧទឧទឧ	TERMIN SET EFF SUMSET ONB SUMSET MIDMIGHT OOB SUMRISE EFF SUMRISE TERMIN RISE ONBIT MOON	0 0 17 29 0 0 22 29 0 0 22 29 0 0 39 60 0 0 57 32 0 0 57 32 0 1 25 1	2 27 19 57 29 3.6 2 27 19 57 29 8.6 2 27 20 14 60 -22.0 2 27 20 32 32 -23.3 2 27 20 32 32 -23.8 2 27 20 37 30 -17.0	-10.2 150.9 -10.2 150.9 49.8 148.7 122.6 143.6	-169.0 31.6 -90.0 31.6 -19.3 31.6 -19.8 31.6 .0 31.6
000000	TERMIN SET EFF SUNSET ORB SUNSET MIDHIGHT ORB SUNRISE EFF SURRISE TERMIN RISE ORBIT HOON	0 1 47 34 0 1 52 34 0 1 52 34 0 2 10 5 0 2 27 36 0 2 32 34 0 2 55 6	2 27 22 2 37 -23.6	-32.7 150.9 -32.7 150.9 27.3 148.7 160.1 148.6 100.1 145.6 118.8 149.1	-160.0 31.7 -160.0 31.7 -90.0 31.7 -19.9 31.8 -19.9 31.8 -0 31.8

SSSS# MAXIMUM LINE MUMBER(

TABLE VIII. - CONTINUED.

			GET				GHT	•				ě	LULH	LULH
ORB		D	HR			D			S	Lat	LON	alt ·		YAY
ৰ		0	3 17			27		52	39		-72.4	151.6	-180.0	31.8
	EFF SUNSET	Ø	3 55			27		57		8.9	-55.2	150.9	-163.0	31.9
4		0	3 55			27	23		40	8.0		150.9	-169.0	31.9
4	***************************************	Ø	3 40			27		15	10	-22.4		143.7	-80.0	31.9
4		O	3 57	41		27		32		-23.5		143.G		31.9
	EFF SUMRISE	0	3 57			27		35		-23.5		143.G		31.9
	TERMIN RISE	Ø	4 2			27		37	40	-18.5		149.1		31.9
5	ORBIT NOON	C	4 25	11	5	23	0	0	11	22.5	173.7	152.0	90.0	31.9
	TERHIN SET	0	4 47			29			44	16.4	-94.9	151.6	-180.0	32.0
5	EFF SUNSET	0	4 52			23	0	27	45	7.7	-77.6		-159.9	32.0
	ORB SUNSET	0	4 52			28	G	27	45	7.7	-77.6	150.9	-159.9	32.0
5		0	5 10		5			45	15	-22.6	-17.5	148.7		32.0
	ORD SUNRISE	0	5 27			23	1		45	-23.3	55.2	148.6	-19.9	32.0
5	EFF SUMRISE	0	5 27		2		1	2	46	-23.3		143.6	-19.9	32.0
	VERNIN RISE		5 32		5		1	7	45	-16.3			0	32.0
6	ORBIT MOON	- 6	5 55	16	2	58	1	30	16	22.7	151.2	152.0	99.0	32.1
	TERMIM SET	0	6 17			23	î	52	49	16.2	-117.4	151.5	-189.6	32.1
	EFF SUMSET	0	8 22			23	1	57	51		-100.1		-159.9	32.1
	ORB SUMSET	. 0	6 22			23	1	57	51		-100.1		-159.9	32.1
6	HIDNIGHT	9	6 40	29		23	2	15	20	-22.8		148.6		32.1
	ORD SUNRISE	0	6 57		2	23		32	50	-23.1		148.5		32.2
	EFF SUMRISE	3	6 57		2		· 2		50	-23.1		143.5	-20.0	32.2
	TERMIN RISE	0	7 2			28			50	-16.1	51.4	149.0		32.2
7	CRBIT NOON	Ø	7 25	21	2	28	3	0	21	22.9	128.8	151.9		32.2

BSRSSB HAXIBUM LINE NUMBERC

TABLE VIII.- CONTINUED.

_																
OF PRIME PAGE IS	000		_		3EŢ	_		_	Gm		_				LULM	LULH
	ORB		Ď	H	M	S	HO	D	Н	F	_5	LAT	LON	ALT	PITCH	YAU
- \$3\$ \$3\$	7		9	?	47	53	S	53	3	55	54	15.9	-139.9	151.5		38.2
がある	ç		0	?	52	56	2	23	3	27	56	7.1	-122.6	150.9		32.2
2 57	7		0	7	52	53	2	23	3	27	53	7.1	-122.6			33.2
<u> </u>	7		9	8	10	24	=	23	3	45	25	-23.0	-62.4	143.6	-୭୭.୭	32.3 32.3
55	7		0	8 8	27	54	2	23	4	2	55	-22.9	10.3	143.5	-23.0	32.3
II T	7		ŏ	_	27 32	54 54	2	23	4	7	55	-22.9	10.3		-20.0	32.3
K M	8		0	8	32 55		2	28	4		54	-15.8	28.9	149.0	.0	22.3
	3	OKDII MOOM	w	ట	55	28	C	53	4	30	26	23.0	106.4	151.9	90.0	32.3
	8	TERNIN SET	0	9	17	53	2	23	4	52	C O	45.3	-462.2	454 5	450.0	
	ន	EFF SUNSET	8	9	53	1	S	SS	4	58	3 <i>9</i>	72.1	-162.3 -145.1	151.5	180.0	32.3
	8	ORB SUNSET	0	9	23	1	S	23	4	58 58	1	5.8		150.9	-159.8	32.4
	ន	mIDNIGHT	0	9	40	29	2	28		15	30	-23.1	-145.1	150.9	-159.8	32.4
	8		9	9	57	59	5	28	5 5		59		-34.8	148.5	-90.0	32.4
	8	EFF SUMMISE	Ö	9	57	59 59	ຣ	23	5		59 59	-22.8	-12.1	148.5	-20.0	32.4
.		TERMIN RISE	8	10	ີຂ	59 59	5	53	5		59 59	-22.8	-12.1	148.5	-20.0	32.4
τω .	9		8			31	5	53	6			-15.6	6.4	149.0	0	32.4
	<i>.,</i>	UNDII HOUH	U	10	63	31	E	20	O	v	31	23.5	84.0	151.9	90.0	32.4
	9	TERHIN SET	0	10	48	3	2	28	6	23	3	15.4	175.2	151.5	180.0	32.5
	ē	EFF SUNSET	ĕ	10	53	6	Ē	23	- G	23	7	6.5	-167.6	150.9	-159.8	32.5
	9	ORB SUNSET	ō		53	န	ຣ	53	ទ	23	7	6.5	-157.5	150.9	-159.8	32.5
	Ð	RIDHIGHT	Õ	11	10	34	2	28	6	45	34	-23.3	-107.2	148.6	-23.0 -23.0	32.5
•	9	ORB SUNRISE	õ		28	ъ <u>э</u>	ຣ	23	7	.3	4	-22.6	-34.G	148.5	-20.0	32.5
•	9	EFF SUNRISE	Õ		53	3	ຣ	28	7	3	4	-22.6	-34.6	148.5	-20.0	32.5
	9	TERMIN RISE			33	4	ž	28	7	8	4	-15.3	-16.1	149.0	.0	38.5
	10	ORBIT NOON	ĕ		55	35	ž	28	7		36	23.4	61.5	151.9	90.0	32.6
			-						•	-, -				20210		22.0

MAXIMUM LINE NUMBERS

		•	G	ET			GH.	ľ					LULH	LULH
ORD		Ð			s no	D	H	n	S	Lat	LON	ค่ะร	PITCH	Vau
10	THRMIN SET	0	12	18	8 8	. 23	7		8	15.2	152.7	151.5		3a.6
10	EFF SUNSET	0	12		s s			53	12	6.2	169.9	150.9		32.6
10	ORB SUNSET	• 0			2 2		7	ទន	12	G.2	169.9	150.5	-159.8	32.6
10	Hidhight	0	12		9 2		8	15	30	-23.5		148.6	-50.0	32.6
0.0	ond sunrise	· 0	12		8 8		8		8	-22.4	-57.0		-20.1	32.6
10	EFF SUMRISE	8	12			23	3		8	-22.4	-57.0		-20.1	32.6
10	Turmin Rise	0	13		ນ ຣ		8	38	9	-15.1	-38.5	149.0	0	32.G
11	OMDIT KOOM	0	13	25 4	0 2	28	9	0	41	23.6	39.1	151.9	89.0	32.7
11	TERMIN SET	0	13	43 1	3 2	28	9	23	13	14.9	130.2	151.5	189.0	32.7
	EFF SUNSET	O		53 1			9				_147.4			32.7
11	CIED SUNSET	. 3	13				9			5.9		159.9	-159.8	32.7
11	HIDHIGHT	• Ø		10 4			9	45	44	-23.7		143.6	-90.0	32.7
11	OND SUNRISE	Ó		28 1	3 2	23	10	Э	13	-22.2	-79.5	148.5	-20.1	32.7
11		0	14	28 1	3 2	23	10	3	13	-22.2	-79.5	148.5	-20.1	32.7
11		0	14	33 1	4 2	28	19	8	14	-14.3	-61.0	149.0	.0	32.8
7'5	OMBIT ROOM	0	14	55 4	5 2	-53	19	30	46	23.7	15.7	151.9	99.0	32.8
12	TERMIN SET	6	15	18 1	8 2	23	10	53	18	14.7	107.7	151.5	180.0	32.8
12	EFF SUMSET	õ	15			23		50	23	5.6	124.9	150.9		32.8
	ONB SUNSET	Õ	15				10		23	5.6	124.9	150.9	-159.7	32.8
12	MIDNIGHT	Ø		40 4					49		-174.5	148.6	-59.0	32.3
12	OWB SUNRISE	0		58 1					17		-101.9	143 5	-20.1	32.9
12	EFF SUMRISE	0		58 1					17		-101.9	143.5	-20.1	32.9
	TERMIN RISE	0		3 1			11	38	19	-14.6		148.9	.0	32.9
13	eabit Moon	0		25 5			12	Ø	51	23.9	-5.7	151.9	80.0°	32.9

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TABLE VIII.- CONTINUED.

			G	ET			GR	7				1 : 1	LULH	LULN
ORD		D	H		HO	D	11	Ħ	S	Lat	LON	ALT		YAH
	TERRIN SET	0	16	48 23	2	28	12	53	23	14.4	85 .3	151.5	180.0	32.9
13	EFF SUNSET	0	16			28	51		ឧធ	5.3			-159.7	32.9
13	ORD SUNSET	0	16	53 28		28	12		23	5.3	102.4		-159.7	33.9
13	ridnight	0		10 54		23		45	54	-24.0	163.1	143.6	-50.0	32.9
13		0					13		22		-124.4	143.5	-20.1	33.0
13	EFF SUMRISE	0	17			28	13				-124.4	148.5	-20.1	33.0
	TERMIN RISE		17			53	13		24		-105.0	140.9	.0	33.0
1.4	ORBIT NOON	0	17	55 55	2	58	13	30	56	24.1	-28.1	151.9	90.0	33.0
1 1	TERMIN SET	a	1 🛭	18 29	ə	28	13	53	28	14.2	62.3	151.5	-180.0	33.0
	EFF SUNSET	õ	18					58		5.0	79.9		-159.7	33.0
14		ŏ	18							5.0			-159.7	33.0
14	HIDHIGHT	ő		49 59			14		59	-24.2			-90.0	33.1
14		ŏ		58 26	_		14		27		-146.8	148.4		33.1
	EFF SUMRISE	_	18			28			27		-146.8		-20.2	33.1
	TERMIN RISE	Ğ	19					38			-123.4		.0	33.1
	ORBIT NOON	õ	19			23			0	24.2		151.8		33.1
		-												
15	TERRIN SET	Ø	19	48 33	2	28	15	23	33	13.9	40.3		180.0	33.1
15	EFF SUNSET	G	19	53 38	2	28	15	23	39	4.7	57.4		-150.7	33.1
15	ORD SUNSET	0	19	53 38	. 2	23	15	53	39	4.7	57.4		-159.7	33.1
15	RIDNIGHT	Ø	2.0	11 4	2	53	15	45	4	-24.3	118.3	148.5		33.2
15	ORB SUMMISE	Ø	29	28 31	2	53	16	3	31	-21.5	-169.3	148.4	-20.2	33.2
15	EFF SUMMISE	0	20	23 31	2	28	16	3	31	-21.5	-169.3	148.4	-20.2	33.2
15	TERMIN RISE	0	20	33 34	. 2	58	16	8	34	-13.8	-150.9		. 0	33.2
16	ORBIT MOON	0	29	58 5	2	23	16	31	5	24.4	-72.9	151.8	99.0	33.2

SSRSS# MAXIMUM LINE NUMBER(

TABLE VIII.- CONTINUED.

			GET			GNT					LULH	LULH
ORB		D	н п	SF	HO D		n s	LAT	LON	ALT	PITCH	YAU
16	TERMIN SET		21 18	38	85 S		33	13.7	17.8	151.5	150.0	33.2
16	eff Sunset		S1 23	44	5 58	16 5		4.4	35.0		159.6	33.2
16	ORD SUMSET		21 23	44	S 58	16 5		4.4	35.0	150.8	-159.6	33.2
16	THDINGIR		21 41	3		17 1		-24.5	95.9	148.6	-50.0	33.3
16	ORD SUNRISE		21 53	35 35	5 58 5 58	17 3 17 3	3 36 3 36	-21.3 -21.3	168.3 168.3	148.4 148.4	-20.2 -20.2	33.3 33.3
16 16	EFF SUMMISE TERMIN RISE		55 3 51 33	38			S 35		-173.4	148.8	6	33.3
17				10			1 10	24.6	-95.3	151.8	90.0	33.3
. 2.1	CREAT MOON	•	الانبا متب	10		2.0	* **	0. T C	23.3	101.0	20.0	
17	TERMIN SET	0	22 43	43	S 28	18 2	3 43	13.4	-4.7	151.5	180.9	33.3
17	EFF SUNSET		22 53	49	2 23	18 2		4.1	12.5	150.8	-159.6	33.3
17	ORB SUMSET		22 53	49	5 58	18 2	8 49	4.1	12.5	150.9	-159.6	33.3
17	TROUNDIN	0	23 11	14	S 58		6 14	-24.6	73.5	148.6	-63.0	33.4
17	ORB SUNRISE			49	S S 8		3 40	-21.1	145.3	148.4	-20.2	33.4
17	EFF SUNRISE		23 28	40	S 53		3 40	-21.1	145.8	148.4	-20.2	33.4
17			23 33	44	S S S		8 44	~13.3	164.1	148.8	.0	33.4
18	orbit Moon	0	23 56	15	5 53	19 3	1 15	24.7	-117.7	151.8	90.0	33.4
4.0	PERMIN ACE		0.40	40	2 22	40 6	7 40	40.4	22.4	454 6	_193 0	33.4
	TERNIN SET	1	0 18 0 23	48 54	S 58 S 58	19 5 19 5		13.1 3.8	-27.1 -10.0	150.8	-180.0 -159.6	33.4
18	EFF SUNSET	4		54	5 58		8 54	3.8	-10.0	150.8	-159.6	33.4
13	HIDNIGHT	4	0 41	19	5 5 5	20 1		-24.8	51.1	148.6	-90.0	33.5
18	ORD SUNRISE	• 🕯	0 53	45	5 58	20 3		-20.9	123.4	143.4	-20.3	33.5
18	EFF SUMRISE	î	0 58	45	5 53	20 3		-20.9	123.4	148.4	-20.3	33.5
18	TERMIN RISE	ī	1 3	48	S 58	29 3		-13.0	141.6	148.8	0	33.5
19	ORDI'I NGON	1	1 26	59	5 58		1 20	24.9	-1.10.1	151.8	80. <u>0</u>	33.5
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TABLE VIII. - CONTINUED.

			GET				GFIT	7					LULH	LULH
ORB		D	ห ็ต		mo	D	Н	Ħ	S	LAT	LON	alt	PITCH	หลย
	TERMIN SET	1	1 48	-	ē	23	21	23	53	12.9	-49.6		-130.0	33.5
19	EFF SUNSET	î	1 53		S	23	21	23	60	3.5	-32.5		-159.6	33.5
19	ORB SUNSET	÷	1 53		2	28	21	28	GÖ	3.5	-32.5		-159.6	33.5
19	HIDHIGHT	1	5 11		ž		21	45	2~	-24.9	28.7	143.6	-80.0	33.6
19	ORB SUNRISE	1	2 23			23	22	3	40	-20.7		148.4		33.6
19	EFF SUNRISE	î	2 28	49		23	22	3	49	-20.7		143,4		33.6
	TERMIN RISE	•	2 33					3	54	-12.7	119.2	148.8	• 3	33.6
	MOCM TIGHO	ī	2 53			28	22	31	25		-162.5	151.8	90.0	33.6
50	ON DIT 110 OH	7	L 50		_									
20	TERMIN SET	i	3 18	57	2	28	22	53	58	12.6	-72.1	151.5	180.0	33.6
50		î	3 24		ā		55	59	5	3.2			-159.5	33.6
63	OAB SUNSET		3 24			28				3.2	-55.0	-150.8		33.6
29	HIDNIGHT	- 1	3 41		ž			16	29	-25.1			-50.0	33.7
	ORB SUNRISE	1	3 58		2		23		54	-20.5	78.5	143.4		33.7
20		1	3 58		5		23			-20.5		148.4		33.7
50	TERMIN RISE	1		58	ž	28	23		59	-12.5	96.7	148.8	.0	33.7
	ORBIT NOON	1	4 26		3	1		1		25.2	175.1	151.8	90.0	33.7
~ I	OKBIT NOON	*	7 66	50		•		•	•	2012				
21	TERMIN SET	1	4 49	2	3	1	0	24	3	12.3	-94.6	151.5	180.0	33.7
	EFF SUNSET	•	4 54		3	1	Ö	59	_	2.9	-77.5	150.9		33.7
is	ORB SUMSET	1	4 54		3	1	Ö		10	2.9	-77.5		-159.5	33.7
21	HIDHIGHT	ī	5 11		3	î		46	34	-25.2	-16.1	148.6		33.7
21	ORB SUNRISE	1	5 28			i	ĭ		59	-20.3	56.0	148.4	-20.3	33.8
57	EFF SUHRISE	. 1	5 28		3	1	î	3	59	-20.3	56.0	148.4		33.8
21	TERMIN RISE	i	5 34		7	1	î	9	4	-12.2	74.2	148.8		33.8
	CRBIT NOON	i	5 58		333	i	•	31	35	25.3	152.7	151.8	90.0	33.8
2 نا	CRD_1 NOON	4	J 30			4	. 4	- 2		2010				

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ISRSSI MAXIMUM LINE MUMBERC

TABLE VIII.- CONTINUED.

ORD 22 TERHIN SET 22 EFF SUNSET 22 ORD SUNSET 22 ORD SUNRISE 22 ORD SUNRISE 22 EFF SUNRISE 22 TERHIN RISE 23 ORDIT HOON	GET D H F 1 6 19 1 6 24 1 6 41 1 6 59 1 6 59 1 7 26	5 FO 7 3 3 3 3 3 3 3 3 3 3 3 3	GHT H S S S S S S S S S S S S S S S S S S	LAT LON 12.0 -117.1 2.6 -100.0 2.6 -100.0 -25.4 -38.4 -20.1 33.6 -20.1 33.6 -11.8 51.7 25.5 130.4	LULH ALT PITCH 151.4 180.0 150.8 -159.5 150.8 -159.5 148.5 -20.0 148.3 -20.3 148.3 -20.3 148.7 .0	LV3 & 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
23 TERMIN SET 23 EFF SUNSET 23 GRB SUNSET 23 MIDNIGHT 23 GRB SUNRISE 23 EFF SUNRISE 23 TERMIN RISE 24 ORBIT NOON	1 8 11 1 8 29 1 8 29	20 3 20 3 43 3 7 3 7 3 13 3	1 3 24 12 1 3 29 21 1 3 29 21 1 3 45 43 1 4 4 8 1 4 9 13 1 4 31 45	11.8 -139.5 2.3 -122.4 2.3 -122.4 -25.5 -60.8 -19.8 11.1 -19.8 11.1 -11.6 29.2 25.6 103.0	151.4 -180.0 150.8 -159.5 150.8 -159.5 148.5 -00.6 148.3 -20.4 148.3 -20.4 148.7 151.7 90.0	99999999999999999999999999999999999999
24 TERMIN SET 24 EFF SUNSET 24 CRD SUNSET 24 MIDHIGHT 24 ORB SUNRISE 24 EFF SUNRISE 24 TERMIN RISE 25 ORBIT MOOH	1 9 24 1 9 24 1 9 41 1 9 59 1 9 53 1 10 4		1 4 54 17 1 4 59 26 1 4 59 26 1 5 16 48 1 5 34 12 1 5 39 18 1 6 1 49	11.5 -162.0 2.0 -144.9 2.0 -144.9 -25.7 -83.2 -19.6 -11.3 -19.6 -11.3 -11.4 6.0 25.7 85.6	151.4 -180.0 150.8 -159.5 150.8 -159.5 148.5 -80.0 148.3 -20.4 148.3 -20.4 148.7	34.0 34.0 34.0 34.0 34.0 34.0 34.0

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TABLE VIII. - CONTINUED.

0 25 25 25 25 25 25 25 25 25 25 25 25 25	eff Sunset orb Sunset Hidhight orb Sunrise eff Sunrise ternin Rise	1 1 1 1 1	GET H H 10 49 10 54 11 11 29 11 29 11 34 11 55	31 53 17 17 23	0 D 3 1 3 1 3 1 3 1 1 3 1	GHT H 849996 44 4 4 9 3 1	5211237 233517 234	LAT 11.2 1.7 -25.8 -19.4 -19.4 -11.1 25.9	175.5 -167.4 -167.6 -33.8 -33.8	ALT 4.0.5 15.0.5	LVLH PITCH 120.0 -150.4 -150.4 -20.4 -20.4 -20.4	LULH YAU . 1 24 . 1 24 . 1 24 . 1 24 . 1 24 . 1 24 . 1
26 26 26 26 26 26 27	EFF SUNSET ORB SUNSET ORB SUNRISE EFF SUNRISE TERMIN RISE	1 1 1 1 1 1 1	12 19 12 24 12 24 12 41 12 59 12 59 13 26	36 36 58 21 21 28	3 1 3 1 3 1 3 1 3 1 3 1	7 54 7 59 7 59 8 16 8 34 8 34 9 1	33 33 58 21 21 23	19.9 1.4 1.4 -25.9 -19.2 -19.2 -10.8 26.0	_170.1 		-159.4	34.1 34.1 34.2 34.2 34.2 34.2 34.2
27 27 27 27 27 27 27 28	EFF & SET ORB SUMSET HIDHIGHT ORB SUMRISE EFF SUMRISE TERMIN RISE	1 1 1 1 1 1	13 49 13 54 13 54 14 12 14 29 14 29 14 34 14 57	41 3 25 26 33	3 1 3 1 3 1 3 1 3 1 3 1	9 24 9 29 9 29 9 47 10 4 10 9 10 32		10.7 1.0 1.0 -25.1 -19.0 -19.0 -10.5 26.1	130.5 147.6 147.6 -150.3 -78.7 -79.7 -60.7		-189.4 -159.4 -159.4 -50.0 -20.4 -20.4 -20.0	344.00000000000000000000000000000000000

#SRSS# MAXIMUM LINE NUMBER C

TABLE VIII. - CONTINUED.

ORD 28 TERNIN SET 23 EFF SUMSET 28 ORD SUMSET 23 MIDNIGHT 23 ORD SUMRISE 28 EFF SUMRISE 28 TERNIN RISE 29 ORDIT NOON	GET S HO 1 15 19 36 3 1 15 24 46 3 1 15 24 46 3 1 15 24 40 3 1 15 59 30 3 1 15 59 37 3 1 16 27	GRT D H H S LAT LON 1 10 54 37 10.4 103.1 1 10 59 47 .7 125.1 1 10 59 47 .7 125.1 1 11 17 8 -26.2 -172.7 1 11 34 31 -18.7 -101.1 1 11 39 38 -10.2 -63.2 1 12 2 9 26.3 -3.9	LULH LULH ALT PITCH VAU 151.4 -180.0 34.3 150.8 -150.4 34.3 150.8 -150.0 34.3 143.5 -20.5 34.3 143.7 -20.5 34.3 143.7 -20.6 34.3
29 TERMIN SET 29 EFF SUNSET 20 ORB SUNSET 20 MIDNIGHT 29 ORD SUNRISE 29 EFF SUNRISE 29 TERMIN RISE 30 ORBIT NOON	1 16 40 41 3 1 16 54 52 3 1 16 54 52 3 1 17 12 13 3 1 17 29 35 3 1 17 29 35 3 1 17 34 42 3 1 17 57 14 3	1 12 24 42 10.1 85.6 1 12 29 52 .4 102.6 1 12 29 52 .4 102.6 1 12 47 13 -26.3 165.0 1 13 4 35 -18.5 -123.6 1 13 9 43 -9.9 -105.6 1 13 32 14 26.4 -26.2	151.4 180.0 34.4 150.8 -159.4 34.4 150.8 -159.4 34.4 148.5 -20.6 34.4 148.3 -20.5 34.4 148.3 -20.5 34.4 148.3 -20.5 34.4 148.3 -20.5 34.4
30 TERMIN SET 30 EFF SUMSET 30 ORB SUMSET 30 ORB SUMRISE 30 EFF SUMRISE 30 TERMIN RISE 31 ORBIT NOON	1 18 19 46 3 1 13 24 56 3 1 18 24 56 3 1 18 42 17 3 1 18 59 40 3 1 13 59 40 3 1 19 4 47 3 1 10 27 18 3	1 13 54 46 9.8 63.1 1 13 59 57 .1 80.2 1 13 59 57 .1 80.2 1 14 17 18 -26.4 142.6 1 14 34 40 -18.3 -146.0 1 14 39 47 -9.7 -123.1 1 15 2 19 26.5 -48.6	151.4 180.0 34.4 150.7 -159.3 34.4 150.7 -159.3 34.4 143.4 -90.0 34.4 143.2 -20.5 34.5 143.2 -20.5 34.5 143.60 34.5 151.6 90.0 34.5

ESRSSE HAXIHUM LINE NUMBERC

			(GET				G:3.	r					LULH	LULH
ORB		D	Н	71	S	mo	D	6-1	Fi	S	Lat	LON	ALT	PITCH	Y A9
31	TERAIN SET	1	19	49	51	3	1	15		51	9.5	40.6	151.4	-190.0	34.5
31	EFF SUNSET	1	19	55	5	3	1	15	30	2	2	57.7	150.7	-159.3	34.5
31	ORB SUMSET	1	19	55	2	. З	1	15	30	2	2	57.7	150.7	-159.3	34.5
31	HIDNIGHT	1	50	12	55	3	1	15	47	22	-26.6	. 120.2	148.4	-90.0	34.5
31	ORD SUNRISE	1	50	20	44	3	1	16	4	44	-18.0	-168.5	148.2	-20.5	34.5
31	EFF SUMRISE	1	20	29	44	3	1	16	4	44	-13.0	-168.5	148.2	-20.5	34.5
31	TERMIN RISE	1	50	34	53	3	1	16	9	52	-9.4	-150.8	148.6	• 0	34.5
35	ORDIT NOOM	1	20	57	23	3	1	16	35	53	26.6	-70.9	151.6	\$0.0	34.5
		_				_									
	TERNIN SET	1	21	19	56	3	_		54		9.2	18.1	151.4	180.0	34.6
32	eff sunset	1	21	25	7	3	1	17	Θ	7	5	35.2	150.7	-159.3	34.6
35	ORB SUNSET	1	21	25	7	3	1	17	0	7	5	35.2	150.7	-150.3	34.6
32	HIDNIGHT	1	21	42	27	3	1	37	17	27	-26.7	97.9	248.4	-90.0	34.6
35	ORD SUMRISE	1	21	59	49	3	1	17	34	49	-17.8	169.1	143.2	-20.5	34.6
32	EFF SUMMISE	1	21	59	49	3	1	17	34	49	-17.8	169.1	148.2	-20.5	34.6
32	TERMIN RISE	1	23	4	57	3	1	17	39	57	-9.1	-173.1	148.6	.0	34.6
33	NOON TIERO	1	55	27	28	3	1	18	2	58	26.7	-93.3	151.5	. 89.0	34.6

8 2260 -LOPT , LAND :

TABLE IX.- FLIGHT 7 NONPROPULSIVE CONSUMABLES LOADING

System	Weight, lb
G02	66.0
GN2	212.0
Potable H ₂ O	578.3
Waste H ₂ O	160.0
NH ₃	97.6
Cryogenic O ₂	1574.0
Cryogenic H ₂	186.0
APU N2H4	1050.0
Hydraulic H ₂ O	428.4
Pressurants	533.0
Total	4885.3

TABLE X.- FLIGHT 7 PROPULSIVE CONSUMABLES LOADING

(a) Minimum RCS propellant budget

Propellant usage, 1b	Forward	After	Total
ET sep (4 fps)	. 57.2	114.5	171.7
Orbit trim maneuvers (15 fps)	4.5	406.3	410.8
PL sep (3.0 fps)	96.9	75.5	172.4
Additional prop for ascending node PL sep	47.0	69.0	116.0
Attitude maneuvers	425.3	956.5	1381.8
Deorbit maneuvers	0.0	1181.2	1181.2
Total usable required	630.9	2803.0	3433.9
Trapped, display and control	492.0	942.0	1434.0
Total required	1122.9	3745.0	4867.9
Total load	1601.0	3760.0	5361.0
Margin ^a	478.1	15.0	493.1

^aMaximum RCS load available = 7508 pounds.

TABLE X.- Continued

(b) OMS propellant budget

Case I (Mi	ssion with	payload at 1	Case II (Case II (Mission without payload at landing)				
	ΔV, fps	Oxidizer, lb	Fuel, 1b	Total, lb	ΔV, fps	Oxidizer, lb	Fuel, 1b	Total, 1b
	211	3 245	1967	5 212	211	3 245	1967	5- 212
Insertion	169	2 495	1512	4 00 6	238	3 319	2012	5 331
Onorbit Deorbit	297	4 236	2568	6 804	273	3 185	1931	5 116
Total usable required	677	9 976	6047	16 022	722	9 749	5910	15_659
		454	312	766		452	306	758
Total trapped		584	. 307	891		584	307	891
		11 014	6665	17 679	1	10 785	6522	17 307
Total required Total load		11 021	6679	17 700		11 021	6679	17 700

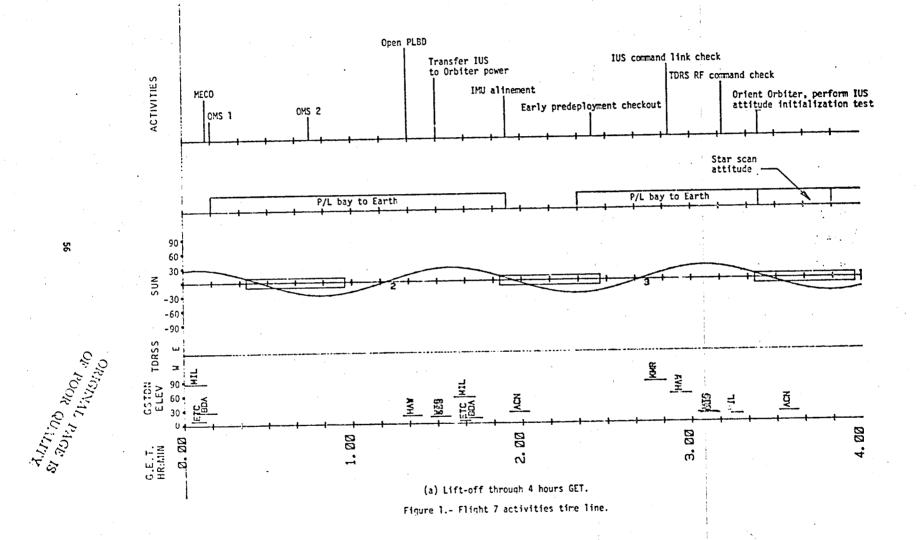
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TABLE X.- Concluded

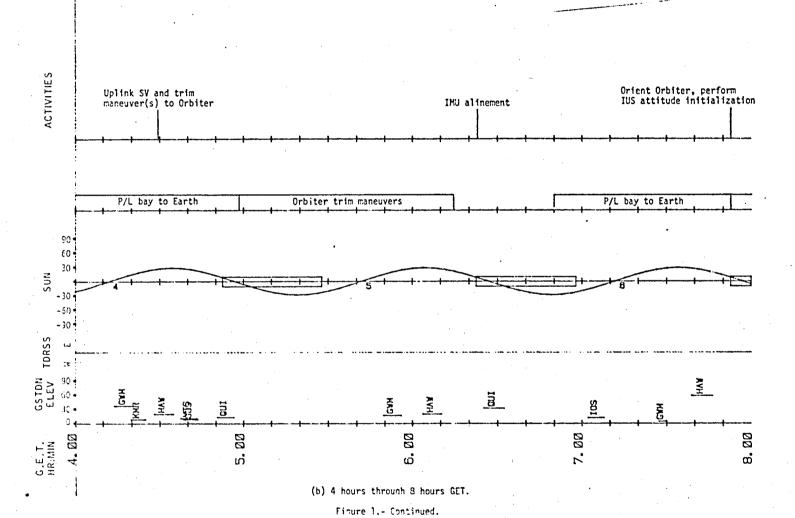
(c) Orbiter mass properties during the mission

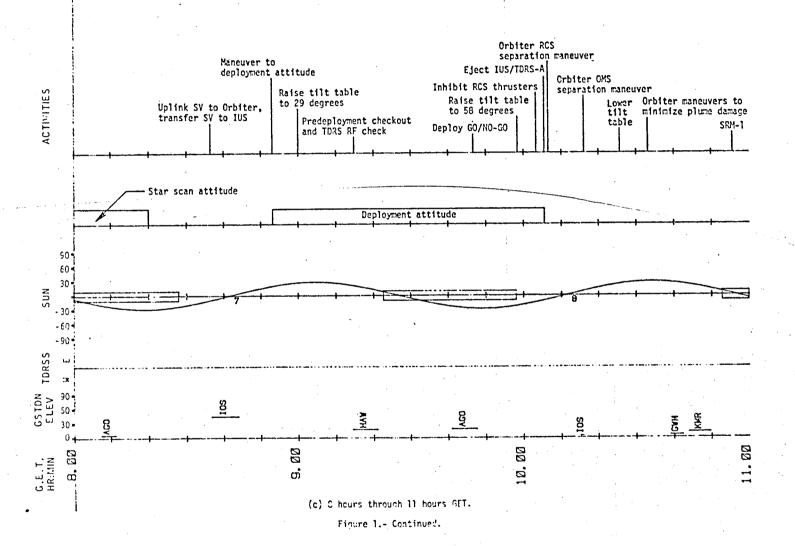
Case	I (Mission with	payload at	Case II (Mission without payload at landing)					
	Weight, 15	X _{cg} , in.	Y _{cg} , in.	Z _{cg} , in.	Weight, 1b	X _{cg} , in.	Yeg, in.	Z _{eg} , in.
Lift-off	251 908.6	1119.4	-0.2	382.8	251 908.6	1119.4	-0.2	282.8
OP CMS-1	251 550.8	1119.4	2	382.8	251 550.8	1119.4	-0.2	382.8
OA CMS-1	246 338.3	1113.3	2	380.8	246 338.3	1113.3	-0.2	380.8
OP CMS-2	240 928.3	1107.0	3	381.4	240 928.3	1107.0	-0.3	381.4
OA CMS-2	236 921.4	1101.7	3	379.8	236 921.4	1101.7	-0.3	379.8
OP PL deployment					235 485.6	1101.7	-0.4	379.4
OA FL release		٠			194 140.6	1113.1	0.0	376.3
OP PL sep burn		e Vita			193 999.7	1113.5	0.0	376.2
OA PL sep burn					192 675.9	1111.3	0.0	375.6
OP deorbit burn	234 261.8	1102.4	-0.3	379.5	191 400.4	1112.2	0.0	375.5
OA ceorbit burn	227 458.1	1092.2	-0.3	376.6	186 284.6	1103.1	0.0	372.8
Entry interface	225 804.7	1090.7	-0.3	376.0	184 631.2	1101.3	0.0	372.1

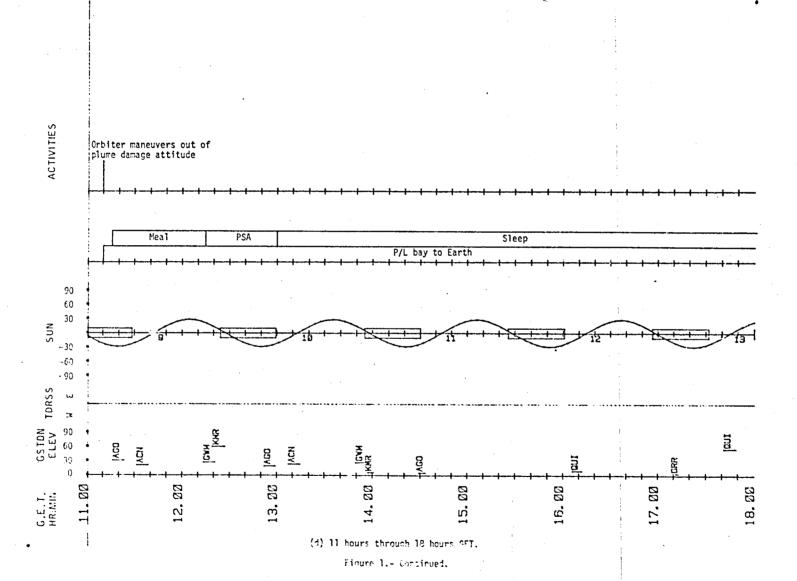
OF = Orbiter prior. OA = Orbiter after.

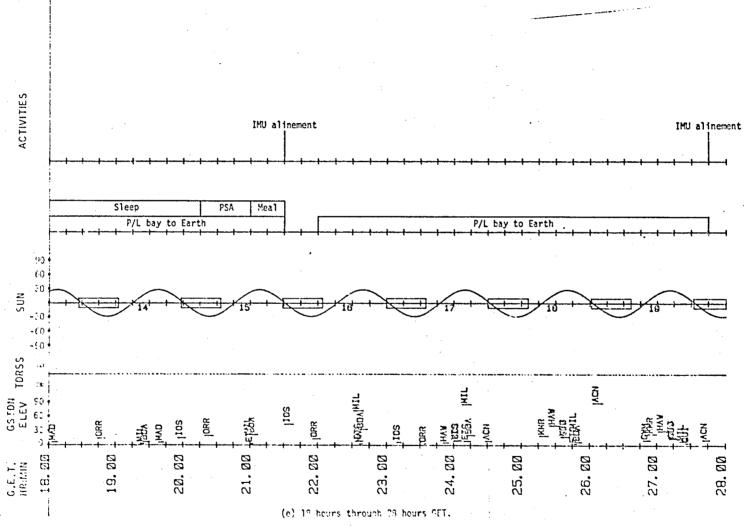












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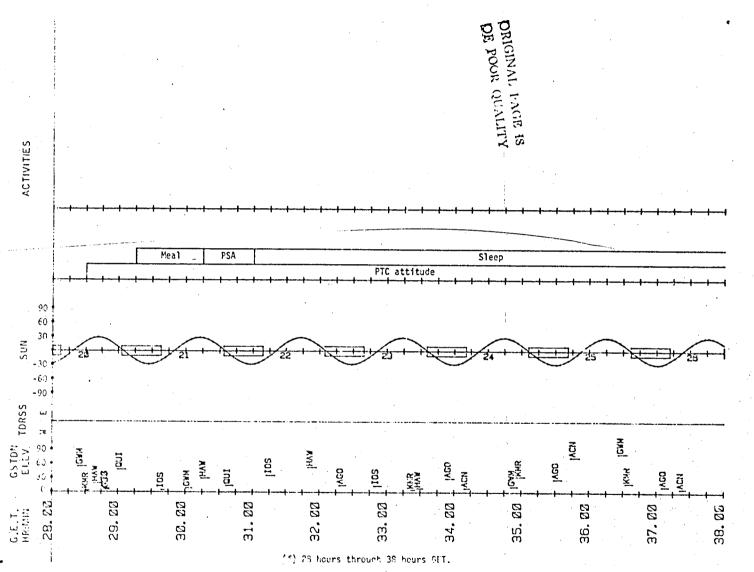
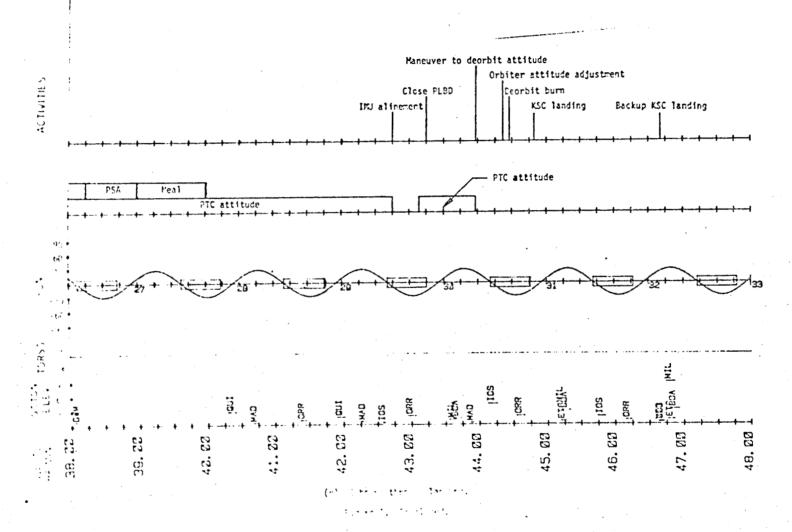
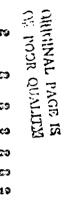
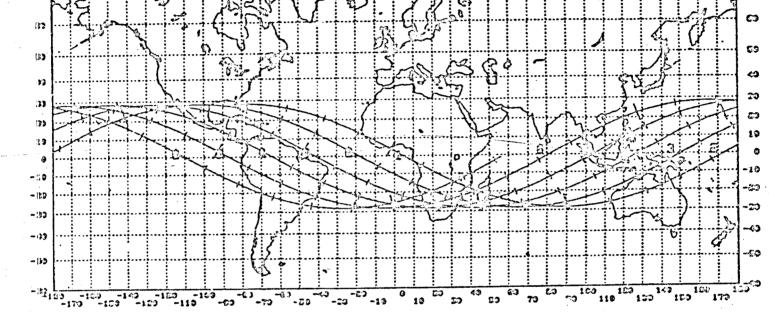


Figure 1.- Continued.

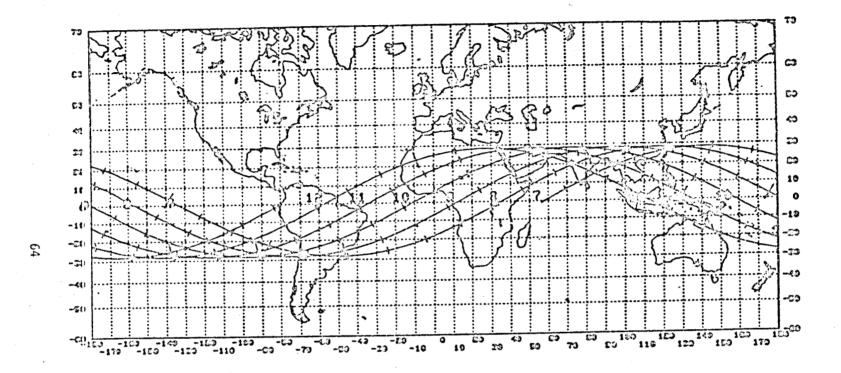




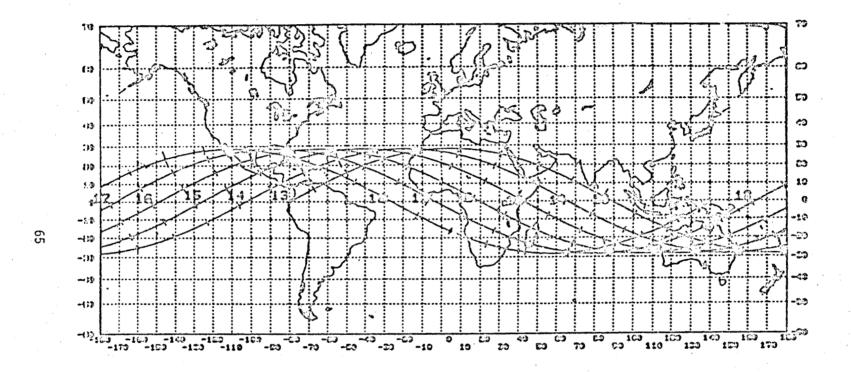


(a) lift-off through orbit 6.

Figure 2.- Orbiter groundtracks

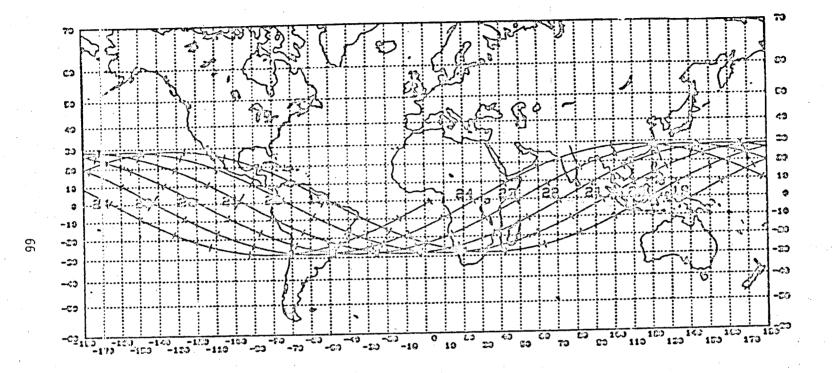


(b) Orbit 6 through orbit 12.
Figure 2.- Continued.



(c) Orbit 12 through orbit 13.

Figure 2.- Continued.



(d) Orbit 13 through orbit 24.

Figure 2. - Continuad.

(e) Orbit 24 through orbit 20.

Figure 2.- Continued.

(f) Orbit 30 through landing.

Figure 2.- Continued.

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Figure 3.- Flight 7 composite launch window.

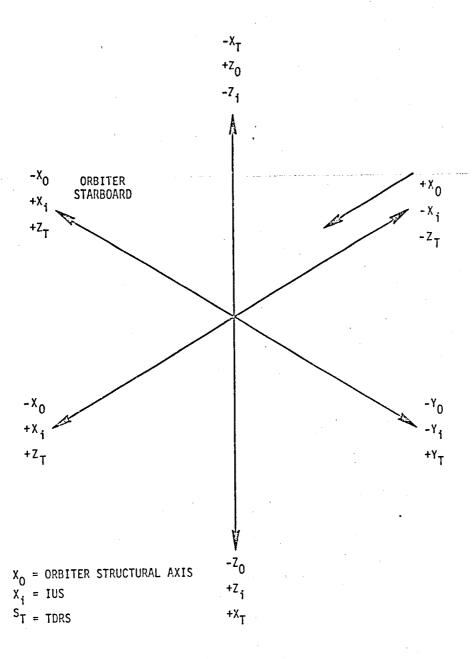
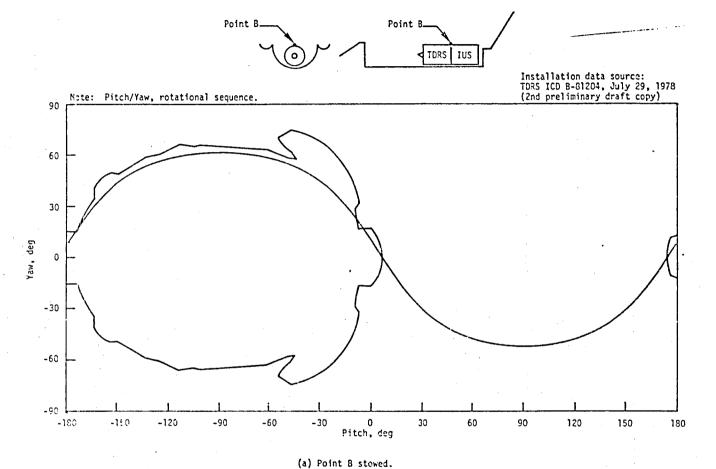
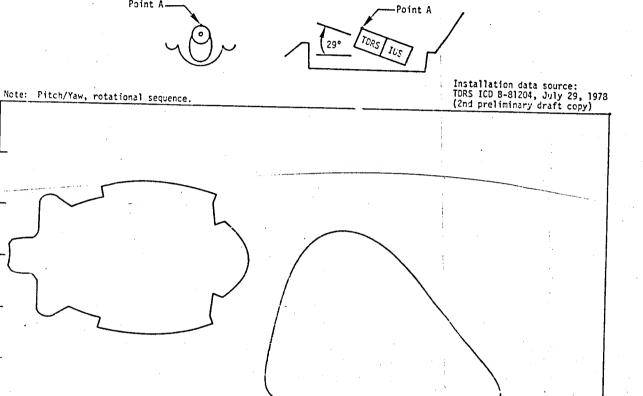


Figure 4.- Definition of orbiter, IUS, and TDRS coordinate systems.



71

Figure 5.- Orbiter blockage map for TDRS/IUS.



Point A-

60

30

-30

-60

-90 -180

-150

-120

-90

-60

(b) Point A elevated.

O Pitch, deg

30

60

90

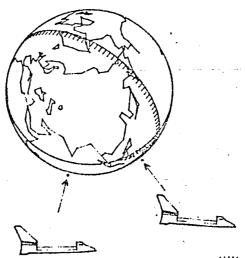
120

150

180

-30

Figure 5.- Continued.



MAN. TO -2 LV G.E.T. 1 0 0.0 P- 42.1 Y- 0.0 R- 160.0

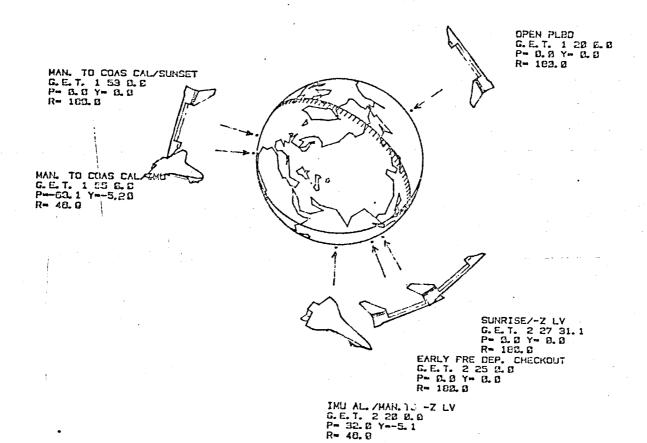
OMS-2 CUTOFF/COAST G.E.T. 0 45 43.0 P--15.1 Y- 0.0 R- 180.0

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane --Due east is ascending node

--Ticks denote earth darkness --β≤0° shows sun as """

Figure 6.- Onorbit pictorial summaries. Orbit No. 1 - (node to node)

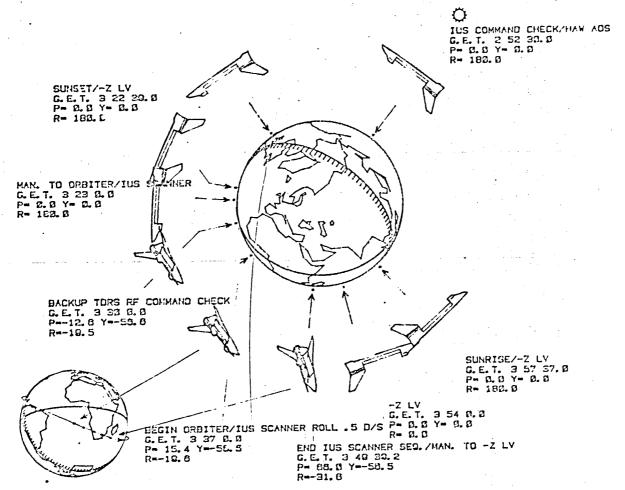


LEGEND: Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Roll

-- View is rerpendicular to orbit plane --Due east is ascending node

--Ticks denote earth darkness --β≤0° shows sun as ""

Figure 6.- Continued. Orbit No. 2 - (node to node) TDRS RF COMMAND CHECK G.E.T. 3 12 0.0 P= 0.0 Y= 0.0 R= 100.0



VIEWED PARALLEL TO ORBIT PLANE

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, 2011

--View is perpendicular to orbit plane
--Due east is ascending node
--Ticks denote earth darkness
--β≤0° shows sun as "O"

Figure 6.- Continued.
Orbit No. 3 - (node to node)

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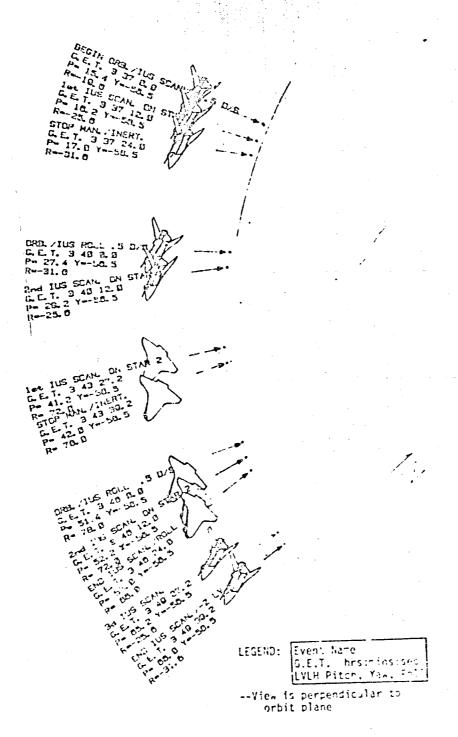
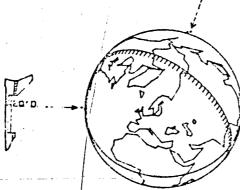


Figure 6.- Continued. Orbit No. 3 - (node to node)

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UPLINK S.V./PERFORM TRIM MAN. G.E.T. 4 20-9. D P= G.G Y= E.B R= 160. B

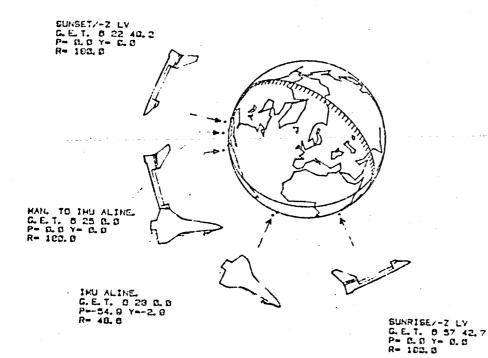
PERFORM TRIM MAN. 1F TEO'D.
G.E.T. 4 57 C.B
P= 0.0 Y= 0.B
R= 100.B



LEGEND: Event Name
G.E.l. hhs:minsise
LVLH Pitch, Yaw. Gr

--View is perpendicular to orbit plane --Due east is ascerding rod --Ticks denote earth trevels, --B≤C° shows sun as ○

Figure 6.- Continued. Orbit No. 4 - (node to node) .

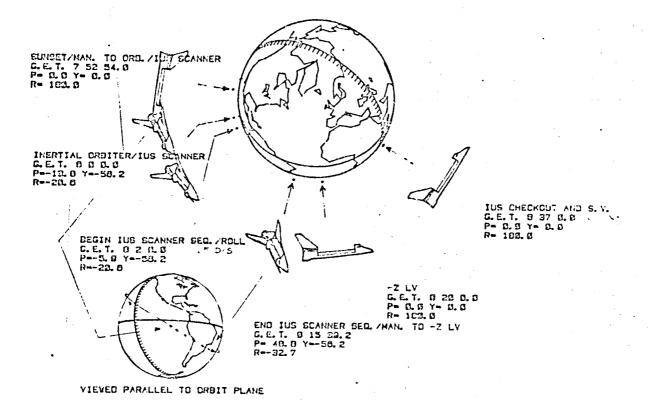


END IMU ALINE./MAN. TO -Z LV G.E.T. 0 45 E.0 P= 13.1 Y=-2.8 R= 46.0

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Foll

--Yiew is perpendicular to orbit plane --Due east is ascending node --Ticks denote earth darkness --β≤0° shows sun as 'O'

Figure 6.- Continued.
Orbit No. 5 - (node to node)



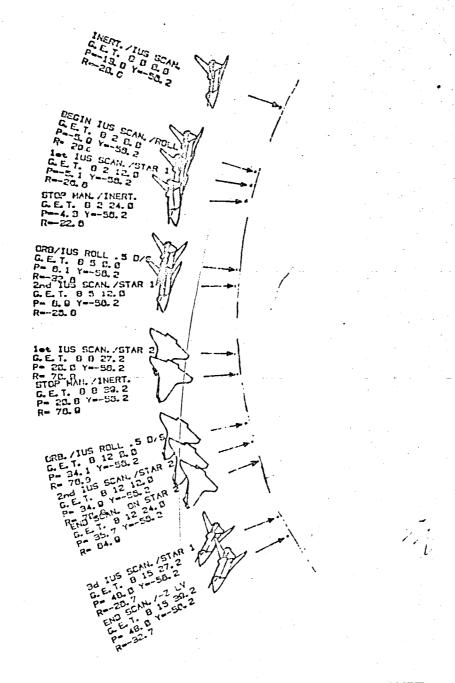
LEGEND: Event Name

G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Poll

--View is perpendicular to orbit plane -- Due east is ascending node

--Ticks denote earth dirkness $--\beta \le 0^\circ$ shows sun as " \circ "

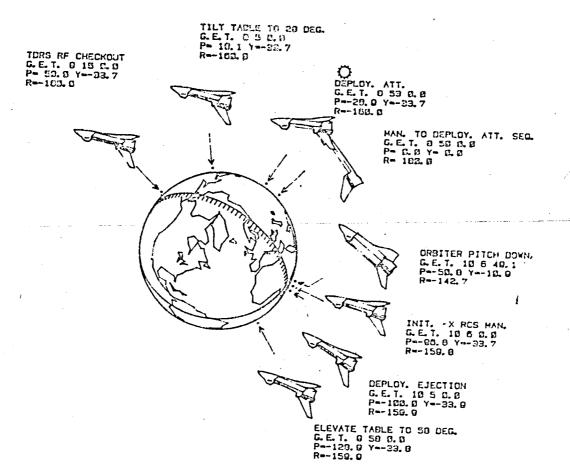
Figure 6.- Continued. Orbit No. 6 - (node to node)



LEGEND: Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane

Figure 6.- Continued. Orbit No. 6 - (node to node)



LEGEND: Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Roll

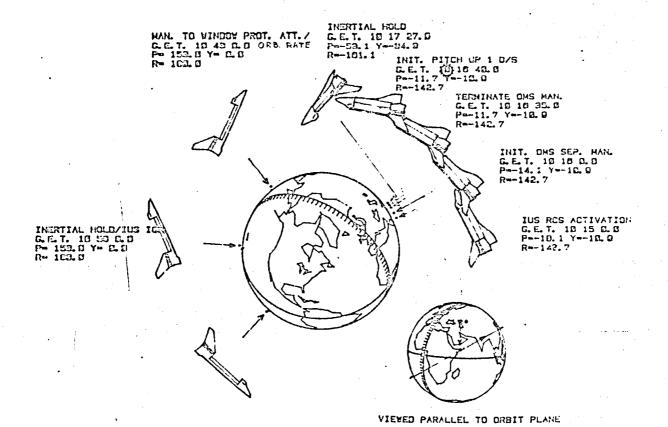
--View is perpendicular to orbit plane

-- Due east is ascending node

--Ticks denote earth darkness --β≤0° shows sun as "O"

Figure 6.- Continued. Orbit No. 7 - (node to node)

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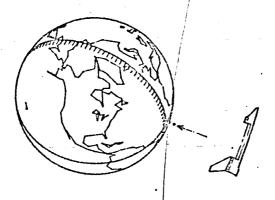


-Z LV G.E.T. 11 18 6.8 P= C.8 Y= C.8 R= 188.8

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane
--Due east is ascending node
--Ticks denote earth darkness
--β≤0° shows sun as "o"

Figure 6.- Continued.
Orbit No. 8 - (node to node)



DEGIN SLEEP C.E.T. 13 10 C. 0 P= C. 8 Y= C. 0 R= 160.0

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane
--Due east is ascending node
--Ticks denote earth darkness
--β≤0° shows sun as "♥"

Figure 6. - Continued. Orbit No. 9 - (node to node)

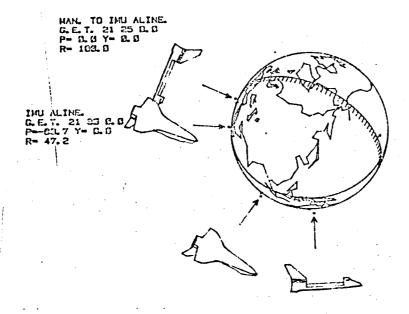


END SLEEP/-Z LV G.E.T. 20 15 C.O P- B.O Y- B.O R- 100.0

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane --Due east is ascending node --Ticks denote earth darkness --β≤0° shows sun as """

Figure 6.- Continued. Orbit No. 14 - (node to node)



END INU ALINE /MAN. TO -Z LV G.E.T. 21 45 8.8 P=-0.0 Y= 2.1 R= 47.2

C.E.T. 21 55 6.6 P- 8.8 Y- 8.8 R- 168.6

LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane

-- the east is ascending node -- Ticks denote earth darkness -- $\beta \le 0^\circ$ shows sun as " \bigcirc "

Figure 6.- Continued. Orbit No. 15 - (node to node)

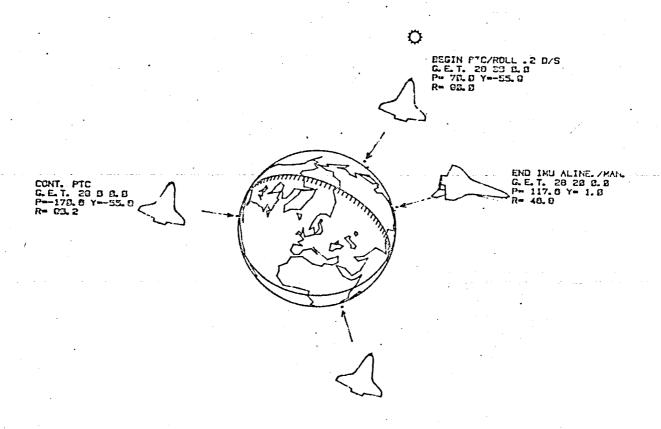
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LEGEND: Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Poll

- --View is perpendicular to orbit plane
 --Due east is ascending node
 --Ticks denote earth darkness
 --β≤0° shows sun as "♥"

Figure 6.- Continued. Orbit No. 19 - (node to node)



CONT. PTC G.E.T. 20 20 8.8 P=-52.5 Y=-55.8 R= 98.3

LEGEND: Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane
--Due east is ascending node
--Ticks denote earth darkness
--β≤0° shows sun as "♥"

Figure 6.- Continued. Orbit No. 20 - (node to node)

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)

END IMU ALINE. /MAN. G.E. T. 29 23 2.8 P- 117.6 Y- 1.8 R- 46.8 CONT. PTC
G.E. T. 23 42 E.0
P=-132.0 Y=-55.7
R=-149.5

Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Roll

is perpendicular to pit plane east is ascending node denote earth darkness shows sun as ""

Figure 6.- Continuarian.
Orbit No. 21 - (nece to man



END SLEEP G.E.T. 39 15 E.B P-127.1 Y-55.3 R-67.7

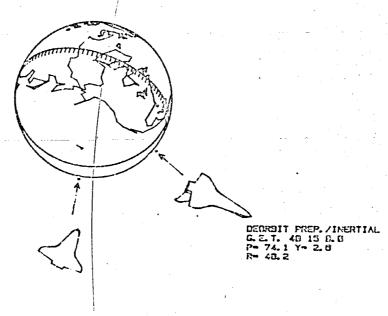
LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

- --View is perpendicular to orbit plane
 --Due east is ascending node
 --Ticks denote earth darkness
 --β≤0° shows sun as "";"

Figure 6.- Continued.

Orbit No. 25 - (node to node)

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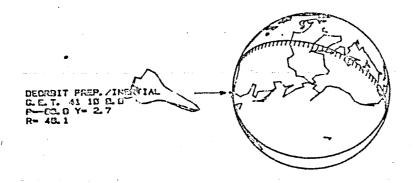
END PTC/MAN. TO INU G.E.T. 43 B C.B P-711 G Y-51.2 R- 62.7

LEGEND: Event Name G.E.T. hrs:mins:secs LVLH Pitch, Yaw, Roll

- --View :s perpendicular to orbit plane --Due east is ascending node --Ticks denote earth darkness --β≤0° shows sun as "O"

Figure 6.- Continued.

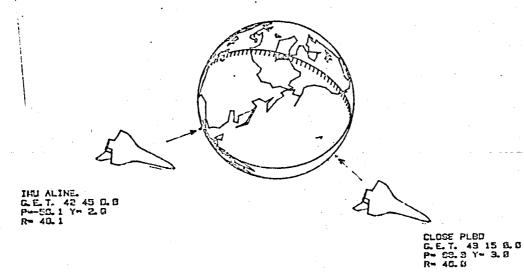
Orbit No. 26 - (node to node)



LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane
--Due east is ascending node
--Ticks denote earth darkness
--β≤0° shows sun as "O"

Figure G.- Continued. Orbit No. 27 - (node to node)



LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

--View is perpendicular to orbit plane
--Due east is ascending node
--Ticks denote earth darkness
--β≤0° shows sun as "○"

Figure 6.- Continued.
Orbit No. 28 - (node to node)

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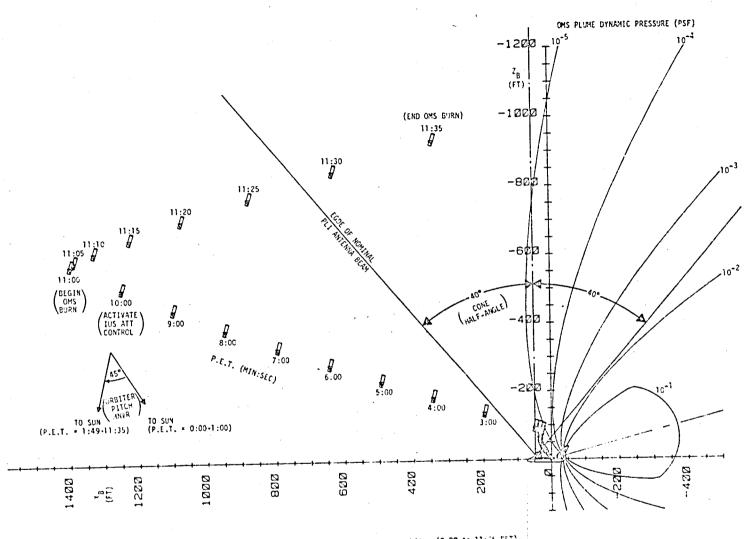
LEGEND: Event Name
G.E.T. hrs:mins:secs
LVLH Pitch, Yaw, Roll

View is perpendicular to orbit plane
 Due east is ascending node
 Ticks denote earth darkness
 β≤0° shows sun as "O"

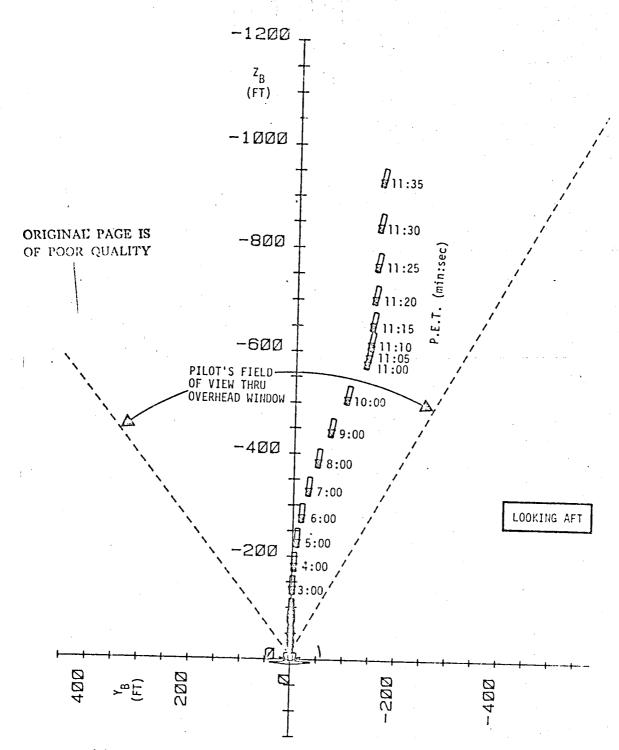
Figure 6.- Concluded.

Orbit No. 29 - (node to node)

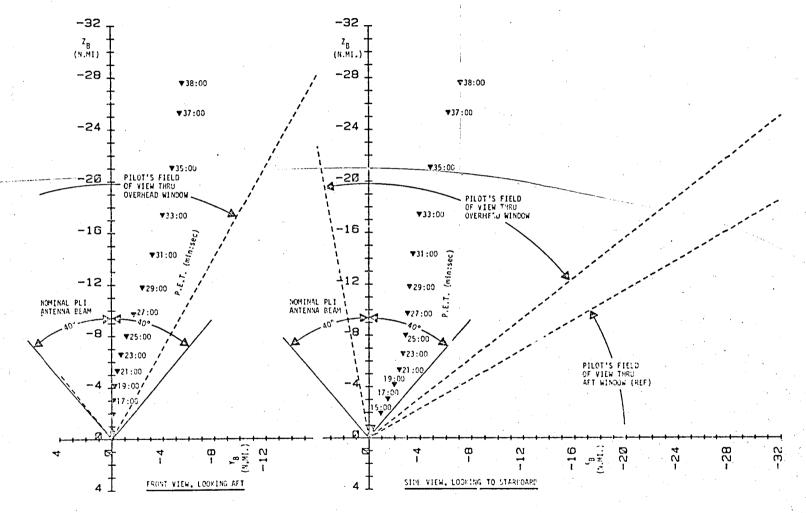




(a) Sideview of payload motion relative to orbiter (n:00 to 11:35 FET)
Figure 7.- Postseparation relative motion between orbiter and IUS (TUDE-F)

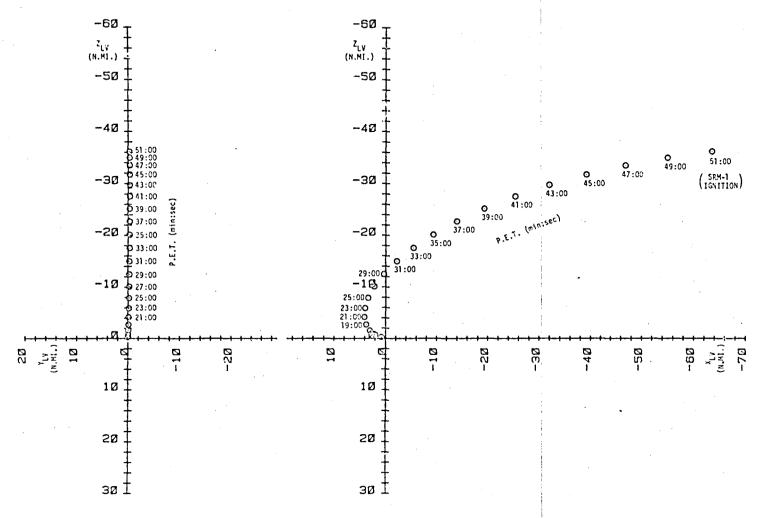


(b) Front view of payload motion relative to orbiter (11:40 to 38:00 PET) Figure 7.- Continued.

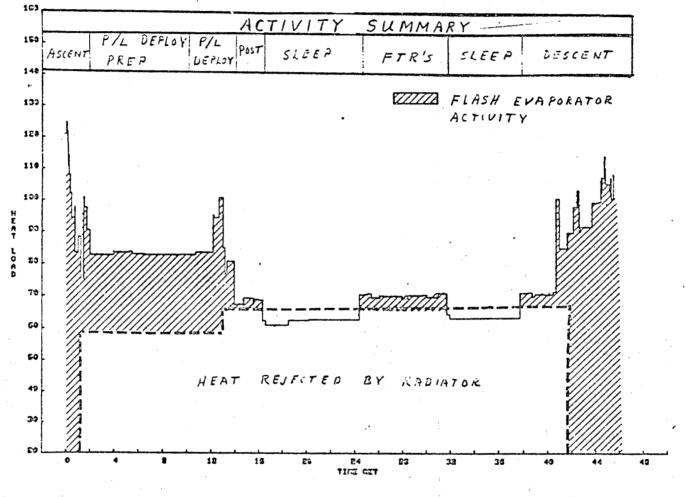


(c) Payload motion relative to orbiter tody axes (11:46 to 30:00 PET)

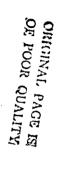
Figure 7.- Continued.

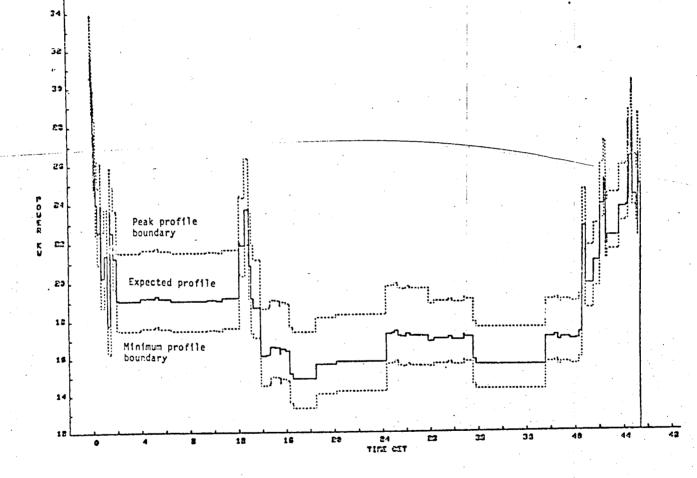


(d) Orbiter LVLH trajectory relative to payload (13:00 to 51:00 PET) Figure 7.- Concluded.

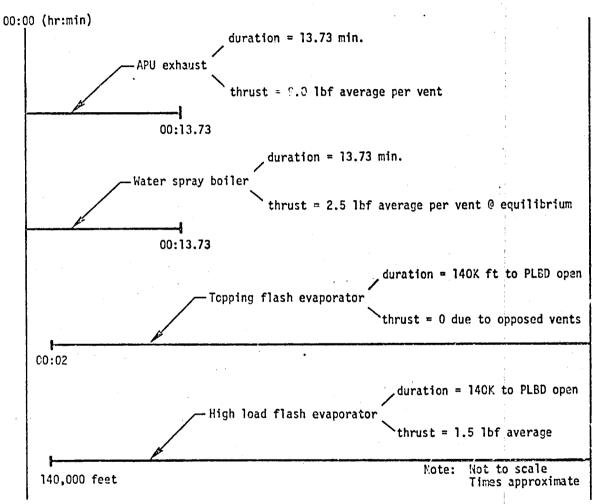


(a) Flight 7 active thermal control system thermal profile.
Figure 8.- Flight 7 nonpropulsive consumables.





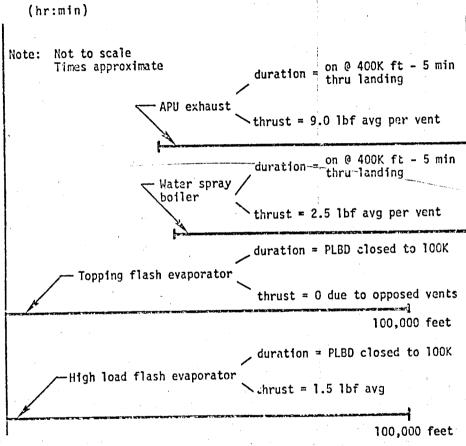
(b) Flight 7-total source power profile.
Figure 8.- Continued.



(c) Flight 7 scheduled venting timeline during ascent.
Figure 8.- Continued.

(d) Flight 7 scheduled venting timeline during onorbit.

Figure 8.- Continued.



(e) Flight 7 scheduled venting timeline during deorbit. Figure 8.- Concluded.

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